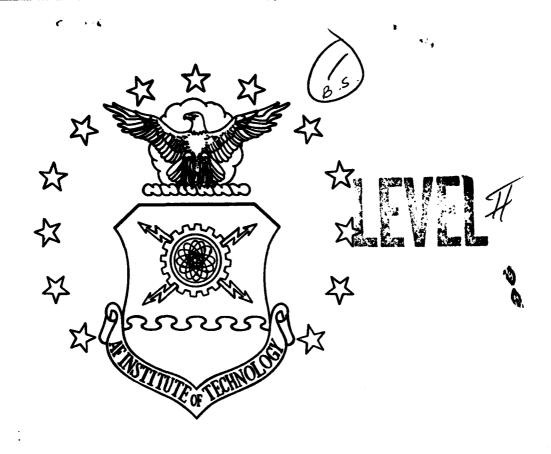
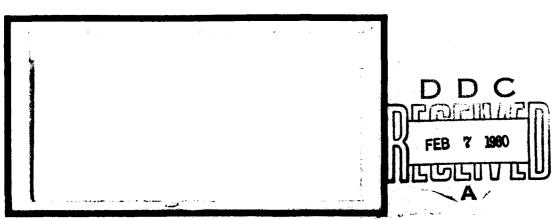
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CROSS VALIDATION OF SELECTION OF VARIABLES IN MULTIPLE REGRESSION

GOR

THESIS

AFIT/MA/79D-2 Joseph R. Cafarella, Jr. 2 Lt USAF

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AFIT/GOR/MA/79D-2

CROSS VALIDATION OF SELECTION OF VARIABLES IN MULTIPLE REGRESSION

Thesis,

Presented to the Faculty of the School of Engineering of the Air Force Institute of Technology

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In Partial Fulfillment of the Requirements for the Degree of Master of Science

/C Joseph R Cafarella, Jr

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Abstract

Techniques and criterion for selection of the "best" subset of variables to be used in a regression model are reviewed.

A model was developed using the Automatic Interaction Detection (AID) algorithm as a pre-screening device for locating those variables most important to the regression including interaction terms.

Five previous models including the one developed by AID and one developed by Westinghouse on avionic characteristic data are used in cross validation experiments to determine the predictive power of these models on a new set of data points using the same set of variables. A cross validation R^2 value is discussed as a criterion for choosing between competing models.

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CROSS VALIDATION OF SELECTION OF VARIABLES IN MULTIPLE REGRESSION

I Introduction

Background

Long term DoD planning goals require than operational and support costs on all projects be reduced. Managers of these projects are challenged by the need for accurate evaluation of these projects in the early design stages. A question arises, however, concerning whether model development and enhancement should be contracted out-of-house or done using available efforts of Air Force personnel in-house. Performing a cost analysis in-house would surely reduce costs. Also, performing an in-house cost analysis would benefit the user of the model by providing first hand knowledge of the impacts of updates and changes in the data base on the final results and may discover intermediate results unknown to a contractor.

One prerequisite for the user to perform in-house analysis is the availability of the necessary computer packages. Another is the knowledge of the user in applying other effective methods of analyzing the goodness of fit of the models other than the R² value or F-statistic discussed in the next chapter. Once the user of the model attains these prerequisites, in-house analysis can be performed.

Since these prerequisites for an in-house capability of cost estimation were not available at the time, the Systems Evaluation Branch (AAA-3) of the Air Force Avion'cs Laboratory at Wright-Patterson Air Force Base requested that the Westinghouse Electric Corporation perform a regression analysis on certain characteristics of Line

Replaceable Avionic Units (LRUs).

The Westinghouse approach was to select "candidate" LRUs for inclusion in the data base, collect data on design and logistic characteristics on the LRUs, perform a regression analysis on the data, then use the resulting cost and parametric relationships to construct a model. The resulting model was named the Avionics Laboratory Predictive Operations and Support (ALPOS) model [36].

One of the problems Westinghouse encountered, which most analysts encounter also, involved the process used in the selection of the data. Probably the most important element in the research is the nature of the data which was used. Many different situations can arise from "bad" data and wrong assumptions about the data such as whether the data subset collected is statistically different from the underlying population or whether multicolinearity exists between variables.

In the initial phase, several LRUs were identified and considered for inclusion in the data base from a wide variety of avionic units placed on various types of aircraft. The LRU selection was naturally constrained by the availability of the data and on the number of aircraft on which the LRU was installed. This initial data base (Phase I) consisted of sixty-three LRUs from seven different aircraft.

For their regression analysis, Westinghouse used the Linear Least-Squares Curve Fitting Program (LLSCFP) developed by Daniel and Wood [8]. This computer program uses over thirty statistics and five types of plots in assisting the analyst develop meaningful variable relationships.

In his Masters thesis, Captain Larry Pulcher attempted to provide the means for the members of AAA-3 to conduct their own in-house cost-estimation analysis by developing and testing criterion for selection of variables in a regression analysis including iterative techniques using the Statistical Package for the Social Sciences (SPSS), all possible regressions using the International Mathematical Statistical Library (IMSL) routine RLEAP, and the Omnitab computer package used to compute prediction intervals.

Both Westinghouse and Pulcher had available a set of potential variables which could be considered for inclusion in the model, however, both sets of variables were too large (more variables than data points). Westinghouse used an approach in which "candidate" variables were screened and tested before admission to the model. Pulcher used a screening technique to eliminate certain candidate variables before hand.

Focus of this Research

Westinghouse has recently updated the data collected in the initial phase. This new Phase II data base includes sixty-five additional LRUs plus six previous ones placed on different aircraft for a total of seventy-one LRUs. Also, four additional aircraft have been included. See Table I for a summary of the LRUs investigated.

One objective of this research is to review past research in the area of selection of variables in a regression analysis in the hope of stimulating thoughts and ideas of those analysts interested in combining talents on this subject.

A second objective of this research is to examine the three previous models developed by Pulcher and the Phase I model developed by Westinghouse and determine which of the models predicts the Phase II data the best.

A third objective of this research is to use the Automatic Interaction Detection (AID) algorithm documented by Sonquist and Morgan [33, 34] to prescreen variables from the entire data set and create a model based on the Phase I data and perform the same predictive tests mentioned above using the Phase II data. A Leaps and Bounds algorithm was used to assess various AID models to determine which one should be represented in the subsequent analysis.

Finally, updated coefficients were calculated for the best predictive model determined in objectives two and three above.

TABLE I
Summary of LRUs Investigated

| Aircraft | PHASE I | PHASE II | TOTAL |
|----------|---------|----------|-------|
| F4E | 11 | 3 | 14 |
| RF4C | 8 | - | 8 |
| F15A | 10 | 20 | 30 |
| В52G/Н | 18 | 1 | 19 |
| KC135A | 5 | - | 5 |
| C130E | 5 | 6 | 11 |
| C5A | 6 | 9 | 15 |
| F106A | - | 2 | 2 |
| F111D | - | 20 | 20 |
| FB111A | - | 10 | 10 |
| TOTAL | 63 | 71 | 134 |

II Concept Overview

Theory of Least Squares Regression

The fundamental premise of a regression analysis is to build a model useful in predicting a single dependent or criterion variable from a set of independent or predictor variables. There are many different types of models which can be created such as general linear discussed in the following section, non linear, logarithmic, polynomial, reciprocal and multiplicative. This research deals mainly with linear, polynomial and logarithmic models.

Assumptions

Before any statistical inferences can be made and tests performed on the significance of the coefficient estimates and the independent variable, certain assumptions must be made about the data and about the probability distribution of the random error.

The first assumption is that the data is a sample from the target population. The second assumption is that the random variable ϵ , the error term, is:

- (1) statistically independent
- (2) identically distributed
- (3) from a population with zero mean
- (4) normally distributed

In other words, $\epsilon \sim N(0, \sigma^2)$ which means that ϵ is from a normal probability density function with a mean of zero and a variance of σ^2 . Also, since nothing is known about the probability distributions describing these error terms, the Central Limit Theorem guarantees that

if we can assume independence, then the sum will tend to be normally distributed. Also, if we can assume that all the error terms have identical probability distributions, then we insure that each of them have the same variance.

Method of Least Squares

The general form of the linear least squares model is

$$Y = \beta_0 + \beta_1 X_1 + \beta_2 X_2 + \cdots + \beta_j X_j + \cdots + \beta_k X_k + \epsilon$$
 (1)

where Y is the observed value of the dependent variable

 $\mathbf{X}_{\mathbf{j}}$ is the observed value of the $_{\mathbf{j}}$ th independent variable

 β_{O} is the constant term

 $\beta_{\mbox{\scriptsize j}}$ is the regression coefficient for the $\mbox{\scriptsize j}$ th independent variable

 ϵ is the random variable accounting for the error

k is the number of independent variables

Note that $X_{\dot{1}}$ can be the transformation of an original observation.

For example, the Product of Powers model

$$Y = \beta_0 X_1^{\beta_1} X_2^{\beta_2}$$
 (2)

can be transformed in a linear sense to

$$ln(Y) = \beta_0 + \beta_1 ln(X_1) + \beta_2 ln(X_2)$$
 (3)

or

$$Y^* = \beta_0 + \beta_1 X_1^* + \beta_2 X_2^*$$
 (4)

where the "*" indicates the transformed variable in equation (4).

If there are n dependent variables, equation (1) can be written:

$$Y_i = \beta_0 + \beta_1 X_{i1} + \beta_2 X_{i2} + ... + \beta_j X_{ij} + ... + \beta_k X_{ik} + \epsilon_i$$
 (5)

where i = 1, 2, ..., n

Since it is very difficult to discuss the multiple regression case in algebraic terms, matrix notation will be used. Equation (5) can be written as:

$$\underline{Y} = \underline{X}\underline{\beta} + \underline{\epsilon} \tag{6}$$

where \underline{Y} represents an n-element column vector of observed values of the dependent variable:

$$\underline{\mathbf{Y}} = \begin{bmatrix} \mathbf{Y}_1 \\ \mathbf{Y}_2 \\ \vdots \\ \mathbf{Y}_n \end{bmatrix} \tag{7}$$

X represents an n x K + 1 matrix. The first column contains all ones representing the constant term. The other columns represent the $X_{i,j}$ values:

$$X = \begin{bmatrix} 1 & x_{11} & x_{12} & \dots & x_{1K} \\ 1 & x_{21} & x_{22} & \dots & x_{2K} \\ \vdots & \vdots & \ddots & \vdots \\ \vdots & \ddots & \ddots & \vdots \\ 1 & x_{n1} & x_{n2} & \dots & x_{nK} \end{bmatrix}$$
(8)

 β represents a K + 1 x 1 column vector of regression coefficients:

$$\underline{\beta} = \begin{bmatrix} \beta_0 \\ \beta_1 \\ \beta_2 \\ \vdots \\ \beta_k \end{bmatrix}$$
(9)

 $\underline{\varepsilon}$ represents the n-element column vector of error terms:

$$\underline{\varepsilon} = \begin{bmatrix} \varepsilon_1 \\ \varepsilon_2 \\ \vdots \\ \varepsilon_n \end{bmatrix} \tag{10}$$

The objective of the least squares technique is to fit a line through a set of data points so that the sume of the squared differences between Y_i (i = 1, 2, ..., n), the actual values of the dependent variable, and \hat{Y}_i , the estimated value of the dependent variable, is minimized.

Y is defined algebraically as:

$$\hat{Y}_{i} = \beta_{0} + \beta_{1} X_{i1} + \beta_{2} X_{i2} + \beta_{j} X_{ij} + \dots + \beta_{k} X_{k}$$
 (11)

or in matrix notation as:

$$\hat{\underline{Y}} = \underline{X}\underline{\beta} \tag{12}$$

The random error term ϵ is the difference between \underline{Y} and $\underline{\hat{Y}}$ and can be written as follows:

$$\underline{\varepsilon} = \underline{Y} - \hat{\underline{Y}} \tag{13}$$

A two-dimensional graphical depiction of a regression line using three data points is shown in Figure 1.

The ideal situation is to have each of the error terms equal to zero. That way, the regression model would fit the data points exactly. In most cases, however, this is not possible so minimizing the sum of the error terms is the best solution. In order to keep the mathematics relatively easy, the error terms are made positive by squaring each term

before summation. This sum of squared errors (SSE) can be written as:

SSE =
$$\sum_{i=1}^{n} (\epsilon_i)^2 = \underline{\epsilon}' \underline{\epsilon}$$
 (14)

where $\underline{\epsilon}'$ is the transposed matrix $\underline{\epsilon}$. The objective can now be stated as follows:

Find β to minimize:

$$SSE = \underline{\varepsilon}' \quad \underline{\varepsilon} = (\underline{Y} - \underline{\hat{Y}})' \quad (\underline{Y} - \underline{\hat{Y}}) = (\underline{Y} - \underline{X}\underline{\beta})' \quad (\underline{Y} - \underline{X}\underline{\beta}) \quad (15)$$

Using a straightforward application of Lagrange's Multipliers on equation (15), one estimator of $\underline{\beta}$ which minimizes SSE is:

$$\hat{\underline{\beta}} = (\mathbf{x}^{\dagger}\mathbf{x})^{-1} \ \mathbf{x}^{\dagger}\underline{\mathbf{y}} \tag{16}$$

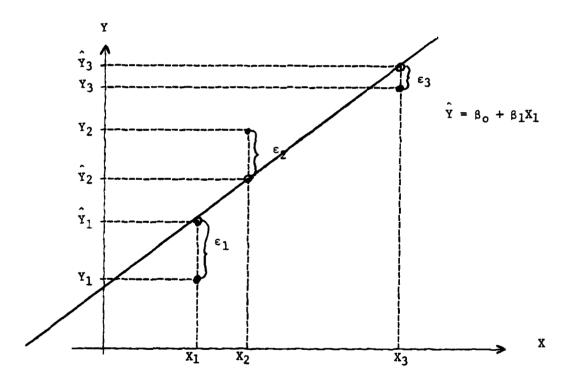


FIGURE 1 Regression Line

It is known, however, that a regression model containing these estimates of $\underline{\beta}$ will not explain all of the variability in the dependent variable \underline{Y} . Some of the variability in \underline{Y} will be explained by the regression model and the remaining portion is left unexplained. This idea can be stated as follows:

$$SST = SSR + SSE$$
 (17)

where SST is the total sum-of-squares or the total variability in the dependent variable and is defined as:

SST =
$$\sum_{i=1}^{n} (Y_i - \overline{Y})^2 = \sum_{i=1}^{n} Y_i^2 - n\overline{Y}$$
 (18)

or

$$SST = \underline{Y}' Y - n \overline{Y}^2$$
 (19)

SSR is the regression sum-of-squares or the variability in the dependent variable explained by the regression model and is defined as:

$$SSR = \sum_{i=1}^{n} (\hat{Y}_i - \overline{Y})^2$$
 (20)

or

$$SSR = \hat{\underline{\beta}}' X' \underline{Y} - n\overline{Y}^2$$
 (21)

SSE is the residual or error sum-of-squares or the remaining amount of variability which is left unexplained and is defined by equation (15).

Measures of Merit:

Since SST depends only on the values of the dependent variables, Y_1 , it is constant for any given set of n observations. Also, since SSE is being minimized, this makes SSR as large as possible. It is then reasonable to assume that the ratio of SSR to SST would be an adequate indicator of the goodness of fit of the model to the data

and a good measure of merit of the regression. This ratio is denoted as R_y^2 , or simple as R^2 , and is called the coefficient of determination or the multiple R-squared value.

$$R^2 = \frac{SSR}{SST} = 1 - \frac{SSE}{SST} \qquad 0 \le R^2 \le 1$$
 (22)

According to Theil [35:178], the sample value of \mathbb{R}^2 is somewhat biased due to the degrees of freedom used in its calculation. Theil suggests that a better measure of merit is $\overline{\mathbb{R}}^2$, defined as the adjusted multiple correlation coefficient.

$$\bar{R}^2 = 1 - (1-R^2) \left(\frac{n-1}{n-k} \right)$$
 (23)

or

$$\bar{R}^2 = 1 - (1 - \bar{R}^2) \left(\frac{n-1}{n-k-1} \right)$$
 (24)

if a constant term is included in the model, or equivalently as

$$\bar{R}^2 = R^2 - (1 - R^2) \left(\frac{k-1}{n-k-1} \right)$$
 (25)

In either of the cases above, \overline{R}^2 is always less than or equal to R^2 . It must be noted, however, that \overline{R}^2 is not an unbiased estimator, though it still has some merit because when the number of variables being estimated, k, becomes large compared to the number of observations or data points, n, it still gives an optimistic picture of the amount of variability in the dependent variable explained by the regression model.

 \bar{R}^2 can also be defined as:

$$\overline{R}^2 = 1 - \frac{MSE}{MST}$$
 (26)

where MSE, mean square error = $\frac{SSE}{n-k-1}$

and MST, mean square total = $\frac{SST}{n-1}$

Thus, MSE = MST* $(1-\overline{R}^2)$, and minimizing MSE maximizes \overline{R}^2 .

Mosier [26] has suggested a measure of merit similar to R^2 which measures the predicting power of a model. Based on a model using the original set of old data (Phase I), the estimated value for each data point, \hat{Y}_1 , was calculated. The cross validation SSE (c.v. SSE) was then calculated by the following equation: c.v. SSE = $\sum_{i=1}^{n} (Y_i - \hat{Y}_1)^2$, where the Y_1 s are the actual (observed) values from the new set of data (Phase II). Notice that the c.v. SSE is not the same as SSE because both Y_1 and \hat{Y}_1 did not come from the same sample.

The c.v. SSE is then used to calculate the cross validation R^2 by c.v. $R^2 = 1 - \frac{\text{c.v. SSE}}{\text{SST}}$. Here, c.v. R^2 indicates the predictive power of the old models on the new data.

III Review of Past Research

There is a considerable amount of literature examining the many efforts that have been made to determine the "best" subset of independent variables that should be included in a regression model so that the amount of unexplained variance in the dependent variable is reduced.

Many criteria for selection of these variable subsets have been examined, yet no one best criterion has been found.

Draper and Smith [10:163] point out two conflicting viewpoints on this subject. At one extreme, all variables could be included in the model for predictive purposes, however, though the values predicted may be reliable, as the number of variables in the model approaches the number of data points or observations, R² will naturally become close to one, thus implying a false sense of importance of the model to the unexperienced analyst.

At the other extreme, the model could include as few variables as possible so that the predictions are still reliable and the costs of maintaining and updating the data base is kept at a minimum. A compromise between these two viewpoints is suggested and is considered to be the "best" approach.

One would like to examine all of the 2^k possible regressions of the dependent variable in the search for the best equation, however, not only would there be computational and time limitations on the computer which make this approach impractical, but there is the remaining problem of specifically defining what is meant by the "best" regression model and when it has been found. This chapter reviews some of the research that has been done in this subject area.

Probably the most well known research on the subject of variable selection and regression analysis is that of Draper and Smith. Four different regression approaches have been devised including all possible regressions, backward elimination, forward selection, and stepwise regression.

In the All Possible Regressions technique, all 2^k possible regressions are considered. Thus a ten variable model would require the examination of 2^{10} or 1024 possible regressions. Each model is ordered by some criterion such as R^2 or \overline{R}^2 and compared. Often for large data bases, it becomes necessary to compute the residual mean square error and assess its magnitude to determine the best cut-off point for the total number of variables in the regression.

Recent research by analysts such as Schatzoff, Tsao, and Fienbert [31] have been able to reduce the number of calculations required from an order of k^3 to k^2 , thus making this technique more practical, yet still relatively expensive to use. However, if the number of variables was reduced by methods such as the Chow test developed by Gregory Chow [7], this method becomes even more practical.

In the backward elimination method, a regression equation containing all possible variables is used as a starting point. A partial-F value is calculated for each variable and if a value is less than some specified tabular value, then that variable is removed from the model. Once a variable is removed from the model it is not susceptible to further consideration. A new regression is then computed and the process continues until no more variables can be eliminated from the model. Although this method is not thought of as the most powerful

methods to use in determining the best regression equation, Mantel [23] supports the method and points out its many advantages.

The forward selection process operates in a reverse manner from the backward elimination procedure. Variables enter the model one at a time until a model has been satisfied. Initially, partial—F statistics and partial correlation coefficients are calculated between each independent variable and the dependent variable. The variable most highly correlated will enter the regression equation. A new regression equation is then calculated and the process continues. Once a variable has entered the regression equation, there is no chance that it will be removed. This, however, is one of its faults. There is no attempt to determine the effect an entering variable has on the existing variables in the model.

In the stepwise regression procedure, however, an examination is made at each stage of inclusion of variables in the model to determine whether any variable or set of variables introduced previously lose their significance due to the introduction of a new variable. Thus, a variable which entered at an earlier stage, yet has been found unimportant due to the inclusion of a new variable, will be detected and removed from the model. For this reason, the stepwise procedure has been determined to be the most powerful regression technique.

In discussing various regression procedures, there are three important points that need mentioning. The first point is that the order of inclusion of the variables in the model is irrelevent. Thus, a variable which entered early in the model does not mean that it is more important than a variable which entered later. The second point

is that there is no guarantee that any of the previous methods will arrive at the best regression model. The third point is that there is also no guarantee that each of the previous methods will arrive at the same model or subset of variables. This is true between any set of regression procedures.

There are many more criterion for selecting variable subsets other than \mathbb{R}^2 or the partial-F statistic. The remaining portion of this chapter is dedicated to mentioning those various research efforts.

Aitken [1] discusses the use of the Mean Square Prediction Error (MSPE) as a criterion for selecting variable subsets if the regression equation is used for prediction purposes rather than description purposes. In the later case, he prefers the use of the conventional \mathbb{R}^2 value as a criterion. Allen [2] also discusses the use of the MSPE for selecting variable subsets.

The MSPE is defined as the expected value of the squared difference between the actual value of the independent variable, Y, and the estimated value, Y. If all dependent variables are used in the regression equation, Aitkin defines the MSPE as follows:

MSPE = E[Y -
$$\hat{Y}$$
]² = $\sigma^2 \left[\frac{n+1}{n} + (\underline{x} - \overline{x}) \right] S_{XX} (\underline{x} - \overline{x})$] (27)

where \underline{x} is a row rector of X, \underline{x} is the vector of means, and S_{XX} is the matrix of cross products of the k independent variables: $S_{XX} = X'X$.

Allen defines the MSPE as follows:

MSPE =
$$E[Y - \hat{Y}] = \sigma^2 + Var(\hat{Y}) + [E(\hat{Y}) + X \beta]^2$$
 (28)

where the last term is the squared bias of prediction and the last two terms together are the Mean Square Error (MSE) of \hat{Y} .

Since the least squares predictor \hat{Y} is unbiased, its variance is $\underline{x}(X'X)^{-1}\underline{x} \sigma^2$. If the last term is dropped, one gets:

$$MSPE_{\mathbf{r}} = \sigma^2 + \underline{\mathbf{x}} \left(\mathbf{X}^{\dagger} \mathbf{X} \right)^{-1} \underline{\mathbf{x}} \sigma^2 \tag{29}$$

which Allen uses for the comparison of other predictors.

Kennedy and Bancroft [22] discuss using the average value of the MSPE over their sample as a criterion:

MSPE* =
$$\frac{1}{n} \sum_{i=1}^{n} \sigma^2 \left[\frac{n+1}{n} + (X_i - \bar{x})' S_{xx} - (X_i - \bar{x}) \right]$$
 (30)
= $\frac{\sigma^2}{n} (n + k - 1)$

where X has been assumed to follow a uniform distribution. Aitken, however, believed it more realistic to assume that all X values were independently and identically distributed. In either case, the objective is to chose the variable subset which minimizes the MSPE. If the subset of variables to be tested is specified in advance or simply fixed, the testing hypothesis becomes:

$$H_0$$
: MSPE - MSPE¹ \geq 0

(31)

 H_a : MSPE - MSPE < 0

where MSPE¹ is the MSPE of the variable subset. If the null hypothesis, H_0 , is not rejected, this means that the subset of variables is not statistically different from that of the total set of data and the subset may be considered for use in a prediction equation. A noncentral F-statistic and test have also been developed by Aitken to estimate (31) depending on the assumed distribution and selection process of the independent variables. In the cases where the variable subsets are unknown, a simultaneous procedure, similar to the forward selection process developed by Draper and Smith, was developed by Garland [15]. In this procedure, variable subsets are chosen based on a central-F approximation to the multiple correlation coefficient.

Helms [16] discusses the use of the Average Estimated Variance (AEV) as a criterion for comparing competing linear models and explains why the Integrated Mean Square Error (IMSE) used as a criterion is not very useful in practice. The technique includes the computation of the AEV for each possible regression and the implementation of a stepwise procedure using the AEV as a criterion rather than R^2 or Mallows' C_p statistic. One advantage of the AEV has over R^2 and C_p is that it automatically incorporates information about the tradeoff between bias and variance when one enters or deletes variables in the model.

Furnival and Wilson [13] discuss a technique for computing the error sum of squares (SSE) for all possible regressions with minimal amount of calculations, and show how it is implemented in a branch and bound technique which they refer to as the Leaps and Bounds technique. This technique is useful in determining the best subset, and without examining all the possible subsets of variables.

The fundamental principal upon which their research is based is that $SSE(A) \leq SSE(B)$ where A is any set of independent variables and B is a subset of A. In other words, it is impossible for any subset of A to have a lower error sum of squares than A. Because of this, SSE(A) can be used as a lower bound in the analysis which means that subsets of A can be ignored in the search for the best given numbered variable subset.

In their technique, two search variations are described: horizontal and vertical. The horizontal variation explains regressions in a probability tree form and in a conventional or natural order so

easily observable. These regressions trees are formed by beginning with all k variables in a regression and branching out on all possible k-l variable subsets. The value of SSE is computed for each of the subsets and the subset with the smallest value will be the "best" k-l variable subset. That subset will not be divided further as it provides a minimum value for that branch. Branching occurs elsewhere in the same manner as above until the best possible k-2, k-3, ..., 1 variable subsets are chosen.

Criterion for selecting these variable subsets is based on either \mathbb{R}^2 , \mathbb{R}^2 , or Mallows C_p statistic. In a similar fashion, Narula and Wellington [25] introduce a branch and bound algorithm using the Minimum Sum of Weighted Absolute Errors (MSWAE) as a criterion for selecting variable subsets and involves the use of linear programming to minimize the sum of the absolute values of the residuals subjected to several constraints.

Andrews [4] discusses the use of regression and model building by medians and also introduces a robust method of analyzing data assumed not to have a Gaussian distribution with errors of equal variances.

Webster, Gunst, and Mason [37] discuss a modified least squares estimation procedure using latent roots and latent vectors of the correlation matrix of the dependent and independent variables. This has been found to be very useful when the matrix of independent variables is nearly singular.

In a more recent article, Park [29] discusses a strategy for selecting subsets of variables from a given linear mixture model developed by Scheffe [32], and applies the MSE as a criteria for screening the variables for model reduction.

In another recent article, Ellerton [11] investigates a method of applying linear programming to determine whether a given subset of variables is adequate in a regression model.

Surprisingly enough, very little cross-communication has been done concerning this very important subject, and I believe a joint analytical effort should be made testing these various criteria against various data bases in order to determine if there is one best method or criterion useful in predicting variable subsets to be used in a regression model.

IV Model Development and Selection of Variables

The Westinghouse Data Base

Senior engineers from Westinghouse collected most of the data in both Phase I and Phase II from on site visits to the Pentagon,

AFLC Headquarters, ATC Headquarters, four Air Logistic Centers (ALCs),
and several Air Force bases. While on site, interviews were conducted
with technicians to verify the appropriateness of the LRUs originally
selected and to identify possible alternatives.

At the completion of the Phase II data collection, the resulting data base contained 134 LRUs (See Appendix A), and thirty-three elements (variables plus indicators per LRU) (see Table II). After various variable transformations and modifications, twenty variables remained.

The first set of variables describe the aircraft type and avionics area and are indicators (zero or one). Three aircraft types including fighter, bomber and cargo and three avionic areas including sensory, communication and navigation were initially coded as follows:

| Bomber | 1 | 0 |
|---------------|---|---|
| Cargo | 0 | 1 |
| Fighter | 0 | 0 |
| | | _ |
| Sensory | 1 | 0 |
| Communication | 0 | 1 |
| Navigation | 0 | 0 |

After additional investigation, the following set of indicator

TABLE II
Westinghouse Data Base Elements

| 1. | Bomber indicator variable (1 indicates Bomber aircraft) |
|-----|---|
| 2. | Cargo indicator variable (1 indicates Cargo aircraft) |
| 3. | Sensory indicator variable (1 indicates sensory avaionics) |
| 4. | Communications indicator variable (1 indicates comm avionics) |
| 5. | Unit Price |
| 6. | Volume (in ³) |
| 7. | Weight (lbs) |
| 8. | Component Count |
| 9. | Percentage Digital Components |
| 10. | Percentage Analog Components |
| 11. | Percentage Electro-Mechanical Components |
| 12. | Percentage Power Supply Components |
| 13. | Percentage Transmitter Components |
| 14. | Percentage Solid State Components |
| 15. | Power Dissipation (watts) |
| 16. | Utilization Factor (Operating hours/flying hour) |
| 17. | Percentage Failures Detected by Automatic Test (BIT/FIT FACTOR) |
| 18. | Number of Integrated Circuits |
| 19. | Number of SRUs in the LRU |
| 20. | Mean Time (flight hours) Between Failures |
| 21. | Mean Time (flight hours) Between Maintenance Actions |
| 22. | Maintenance Manhours - Scheduled (Organizational) |
| 23. | Maintenance Manhours - Unscheduled (Organizational) |
| 24. | Maintenance Manhours - Shop (Intermediate) |
| 25. | Logistic Support Cost - Field |
| 26. | Logistic Support Cost - Special Repair Center (Depot) |
| 27. | Logistic Support Cost - Packaging and Transportation |
| 28. | Logistic Support Cost - Condemnation Replenishments |
| 29. | Training Costs |
| 30. | Percentage LRUs Not Repairable This Station (%NRTS) |
| 31. | Flying Hours (FH) (to normalize MMH and LSC) |
| 32. | Percentage Condemned LRUs |
| 33. | Specialized Repair Activity (Depot) Costs |
| 34. | Quantity per Assembly |
| 35. | Flying hours (to normalize Training costs) |
| | |

variables was used in the regression analysis to denote interactions between aircraft type and avionics area:

LRUs in fighter aircraft navigation systems

LRUs in fighter aircraft sensory systems

LRUs in fighter aircraft communication systems

LRUs in bomber aircraft navigation systems

LRUs in bomber aircraft sensory systems

LRUs in bomber aircraft communication systems

LRUs in cargo aircraft navigation systems

LRUs in cargo aircraft communication systems

LRUs in cargo aircraft sensory systems were not included. The above set of indicators is coded as follows:

| Fighter-Navigation | 1 | 0 | 0 | 0 | 0 | 0 | 0 |
|-----------------------|---|---|---|---|---|---|---|
| Bomber-Navigation | 0 | 1 | 0 | 0 | 0 | 0 | 0 |
| Cargo-Navigation | 0 | 0 | 1 | 0 | 0 | 0 | 0 |
| Fighter-Sensory | 0 | 0 | 0 | 1 | 0 | 0 | 0 |
| Bomber-Sensory | 0 | 0 | 0 | 0 | 1 | 0 | 0 |
| Fighter-Communication | 0 | 0 | 0 | 0 | 0 | 1 | 0 |
| Cargo-Communications | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

The next four independent variables are measures of physical characteristics. The Unit Price is measured in 1976 dollars per LRU and ranges in value from \$153 to \$220,943. The Volume is measured in cubic inches and ranges in value from 30 to 8200. The Weight is measured in pounds and ranges in value from one pound to 8200 pounds. Component Count is the number of electronic components and ranges in value from none to 7638.

The next five independent variables are categories of the different component types including Digital, Analog, Electromechanical, Power Supplies, and Transmitter, and are measured as a percentage of the total number of components having that characteristic. All values range from zero to 100 percent.

The next independent variables, Fraction Solid State, and the number of Integrated Circuits in each LRU are measures of LRU technology, the later ranging in value from zero to 4625.

The sixteenth independent variable is a measurement the Power

Dissipation and is defined as the input power minus the transmit power,

and ranges in value from six to 1640 watts.

The next independent variable represents a percentage of failures in LRUs detected by the Built-In-Test/Fault-Isolation-Test (BIT/FIT).

The last two independent variables are the Specialized Activity (Depot) Costs and the Quantity Per Assembly.

Westinghouse also identified several dependent variables. These include the Mean Time Between Failures (MTBF), the Mean Time Between Maintenance Actions (MTBMA), the Total Maintenance Man Hours per Operating Hour (MMH-UNS/OH), the Maintenance Man Hours in the Shop per Operating Hour (MMH-SHOP/OH), the Total Logistic Support Costs per Operating Hour (LSC-TOT/OH), the Field Logistic Support Cost per Operating Hour (LSC-FLD/OH), the Training Costs per Operating Hour (TRAIN/OH), and the percentage of LRUs not repairable this station (NRTS).

Only one of the dependent variables mentioned above will be used

in the analysis; LSC-TOT/OH. A list of all the variables used in this report and previous reports is contained in Table III.

Previous Models

In this section, five previous models (two developed by Westinghouse and three developed by Pulcher) are discussed.

The first Westinghouse model (Table IV) was based on the Phase I data and second (Table V) was based on the Phase II data. All variables in the first model are in linear form, quadratic form or logarithmic form.

The three models developed by Pulcher are described in Table VI and Table VII. Initially, Pulcher was able to create ninety-seven variables from the Product of Powers model of the form:

The D_i are indicator variables, and their function is to allow for coefficients to be different for subpopulations. For a simplified example, suppose we had:

$$\ln Y = \alpha_0 + \alpha_1 D_1 + \beta_1 \ln X_1 + \beta_{11} D_1 \ln X_1$$
 (32)

For the subpopulation for which $D_i = 0$, the model is:

$$ln Y = \alpha_0 + \beta_1 ln X_1$$
 (33A)

while for the subpopulation for which $D_i = 1$, the model is:

$$\ln Y = (\alpha_0 + \alpha_1) + (\beta_1 + \beta_{11}) \ln X_1$$
 (33B)

Since there were only 63 data points, a method was needed to reduce the number of variables. Pulcher chose the Chow Test (also called the Test of Equality Between Subsets of Coefficients in Two Regressions),

TABLE III

List of Variables - Abbreviations

| Name | Westinghouse | Pulcher | This Report |
|--|--------------|------------|-------------|
| Bomber | IBOM | * | BOMBER |
| Cargo | ICAR | * | CARGO |
| Sensory | ISEN | * | SENSORY |
| Communication | ICOM | * | COMM |
| Navigation-Fighter | * | * | FGTNAV |
| Navigation-Bomber | IBMNAV | * | BOMNAV |
| Navigation-Cargo | * | * | CARNAV |
| Sensory-Fighter | * | SF | FGTSEN |
| Sensory - Bomber | * | SB | BOMSEN |
| Communication - Fighter | IFGCOM | CF | FGTCOM |
| Communication - Bomber | IBMCOM | СВ | вомсом |
| Communication - Cargo | * | COMMC | CARCOM |
| Unit Price | UP | UP | UP |
| Volume | J v j | V | V |
| Weight | W | W | W |
| Component Count | cc | СС | CC |
| Component Density | CD | * | * |
| Power Dissipation | PD | PD | PD |
| Fraction Solid State | FSS | % SS | SS |
| Fraction Digital | FDI | % DIG | DIG |
| Fraction Analog | FAN | % AN | AN |
| Fraction Electromechanical | FEM | % EM | EM |
| Fraction Power Supply | FPS | % PS | PS |
| Fraction Transmitter | RXR | % XMTR | XMTR |
| Fraction BIT/FIT | BIT/FIT | BF | BITFIT |
| Number of Integrated Circuits | IC | * | IC |
| Specialized Repair Activity Costs | SRA | * | SRU |
| Quantity Per Assembly | QPA | * | QPA |
| Logistic Support Cost/ Operating Hour | LSC/OH | LSC/OH | LSC/OH |
| Maintenance Manhours/ Operating Hour | MMH/OH | * | * |
| Mean Time Between Failures | MTBF | * | * |
| Mean Time Between Maintenance Actions | MTBMA | * | * |
| Training Cost/Operating Hour | TRAIN/OH | * | * |
| Not Repairable This Station | NRTS | * | * |

^{*} Not used in the analysis

TABLE IV
Westinghouse Model - Phase I Data

| | $ln (LSC/OH) = b_O + \sum_{i=1}^{21} b_i X_i$ | | | | | |
|----|--|----------------------------------|-----------|--|--|--|
| | $\bar{R}^2 = .8916$ $R^2 = .9283$ F-value - 25.3 | | | | | |
| í | bi | Χį | Partial-F | | | |
| 0 | -8.15108 | | | | | |
| 1 | 3.86111 | (IBOM2857142857) | 36.0 | | | |
| 2 | 3,66533 | (ICAR2698412698) | 31.4 | | | |
| 3 | -4.85271×10^{-1} | (ISEN2539682540) | 3.6 | | | |
| 4 | -2,56663 | (IBOM2857142857)(ISEN2539682540) | 37.2 | | | |
| 5 | -1.66262 | (IBOM2857142857)(ICOM206349206) | 12.2 | | | |
| 6 | -7.67253×10^{-1} | (ICAR2698412698)(ICOM206349206) | 3.2 | | | |
| 7 | 1.27356×10^{-2} | FPS | 6.8 | | | |
| 8 | 2.25967×10^{-2} | (FAN-63.349) | 36.0 | | | |
| 9 | -7.42999×10^{-3} | (FSS-61.138) | 9.0 | | | |
| 10 | 2.38503 | (UF-1.639 | 27.0 | | | |
| 11 | -9.20384×10^{-11} | (UP-133606.3) ² | 25.0 | | | |
| 12 | -1.52864×10^{-4} | (W-64. 314)2 | 8.4 | | | |
| 13 | -1.07105 x 10 ⁻³ | (FAN-48.895) ² | 33.6 | | | |
| 14 | 1.20418 x 10 ⁻³ | (FEM-46.991) ² | 33.6 | | | |
| 15 | 7.10025×10^{-4} | (FXR-40.172) ² | 10.9 | | | |
| 16 | -1.61651 x 10 ⁻⁴ | (FSS-51.898) ² | 2.2 | | | |
| 17 | -1.11568 x 10 ⁻⁶ | (PD-722.249) ² | 7.3 | | | |
| 18 | 5.009996 | (UF-1.681) ² | 42.2 | | | |
| 19 | 1.70042×10^{-3} | (BF-27.288) ² | 13.0 | | | |
| 20 | 4.60293 x 10 ⁻¹ | în(UP) | 31.4 | | | |
| 21 | 2.35583 x 10 ⁻¹ | In(V) | 4.8 | | | |

TABLE V
Westinghouse Model - Phase II Data

| | $ ln (LSC/OH) = b_0 + \sum_{i=1}^{18} b_i X_i $ | | | | | |
|----|---|------------------------|-----------|--|--|--|
| : | $R^2 = .8827$ | F-Value = | 41.0 | | | |
| i | b _i | x _i | Partial-F | | | |
| 0 | -6.97950 | | | | | |
| 1 | 7.85143 x 10 ⁻¹ | IFGCOM | 10.24 | | | |
| 2 | 1.14876 | IBMNAV | 34.81 | | | |
| 3 | 1.07719 | IBMCOM | 21.16 | | | |
| 4 | 1.91500 x 10 ⁻¹ | CD | 12.25 | | | |
| 5 | -1.22007 x 10 ⁻² | FDI | 37.21 | | | |
| 6 | -1.72307 x 10 ⁻² | FEM | 24.01 | | | |
| 7 | -9.49029 x 10 ⁻³ | FXR | 4.84 | | | |
| 8 | -8.36154 x 10 ⁻³ | FSS | 9.61 | | | |
| 9 | -3.35635×10^{-4} | (V-1333.0) | 9.00 | | | |
| 10 | 1.98641 x 10 ⁻² | (W-32.3) | 17.64 | | | |
| 11 | 6.72953 x 10 ⁻⁸ | $(v-3222.0)^2$ | 6.25 | | | |
| 12 | -1.05350 x 10-4 | $(W-65.3)^2$ | 4.00 | | | |
| 13 | -4.24991 x 10-8 | (CC-2986) ² | 5.76 | | | |
| 14 | -4.36525 x 10-4 | $(FPS-45.48)^2$ | 9.61 | | | |
| 15 | 7.79704 x 10 ⁻¹ | $(UF-1.72)^2$ | 16.81 | | | |
| 16 | 5.64131 x 10 ⁻¹ | ln(UP) | 94.09 | | | |
| 17 | 4.61602 x 10 ⁻¹ | ln(V) | 8.41 | | | |
| 18 | 1.47264×10^{-1} | ln(PD) | 6.25 | | | |

TABLE VI Pulcher's SPSS Model - Phase I Data

| $R^2 = 0.95212$ | $\bar{R}^2 = 0.92388$ | F = 33.72 |
|--------------------------------------|--|--|
| $\ln (LSC/OH) = \alpha_O + \Sigma$ i | $\alpha_{\mathbf{i}} \mathbf{p}_{\mathbf{i}} + \sum_{\mathbf{j}} \beta_{\mathbf{j}0} \ln x_{\mathbf{j}} + \sum_{\mathbf{j}} \sum_{\mathbf{j}} \mathbf{p}_{\mathbf{i}}$ | β _{ji} D _i ln x _j |
| Variable No. | Coefficient | Partial F |
| 1 | 0.402702 | 13.63 |
| 3 | 0.084548 | 0.10 |
| 5 | 0.412407 | 37.28 |
| 8 | 11.320694 | 23.80 |
| 10 | -1.135445 | 17.68 |
| 11 | -1.457859 | 26.48 |
| 14 | 3.710527 | 7.25 |

-2.950970

9.44

16

TABLE VII
Pulcher's Leaps and Bounds Models - Phase I Data

| $\ln (LSC/OH) = \alpha_0 + \sum_{i} \alpha_i D_i + \sum_{j} \beta_{j0} \ln x_j + \sum_{j} \sum_{i} \beta_{ji} D_i \ln x_j$ | | | | | |
|--|----------------------|----------------------------|----------------------|------------------------|--|
| | C _p Cr | iterion | R ² Cri | terion | |
| | $\overline{R}^2 = 0$ | 0.9135 0.88347 31.21 | $\overline{R}^2 = 0$ | .9323 .9001 9.25 | |
| Variable | Coefficient | Partial-F | Coefficient | Partial-F | |
| UP | 0.245908 | 8.78 | 0.313871 | 14.52 | |
| w | 0.384075 | 7.75 | 0.350494 | 6.86 | |
| SF | -1.061926 | 12.78 | -2.878942 | 14.29 | |
| SB | -1.822390 | 30.26 | -2.195891 | 39.06 | |
| DIG | | | 4.381530 | 4.88 | |
| nf*w | -0.431742 | 31.61 | -0.343076 | 2.10 | |
| NF*CC | -0.466254 | 13.70 | -0.470354 | 15.84 | |
| NF*PD | 0.738901 | 16.62 | 0.672722 | 14.59 | |
| NC*UP | 0.285409 | 5.13 | 0.254284 | 4.04 | |
| NC*A | -0.334677 | 4.93 | -0.292486 | 3.92 | |
| SF*CC | | | 0.293229 | 6.30 | |
| DIG*UP | -0.584870 | 12.86 | -0.950128 | 11.70 | |
| DIG*V | | | -0.971576 | 2.25 | |
| DIG*W | | | 2.676919 | 4.93 | |
| DIG*PD | 1.081951 | 15.97 | 0.553008 | 2.59 | |
| an*w | 0.309271 | 16.60 | 0.239272 | 9.98 | |
| EM*W | 0.698175 | 13.89 | 0.705835 | 13.47 | |
| EM*PD | -0.555855 | 21.58 | -0.545678 | 20.61 | |
| BF*W | 0.866668 | 28.67 | 0.828916 | 27.04 | |
| BF*%SS | -0.701034 | 37.03 | -0.706378 | 38.19 | |
| Constant | -3.855040 | 53.44 | -4.091618 | 64.16 | |

All other coefficients are zero.

which prescreens the variables and eliminates those which are unimportant. The Chow Test also determines which subpopulation really had different coefficients. Sixty variables remained and were used in conjunction with the three models.

A stepwise regression procedure using SPSS was used to develop the first model and the Leaps and Bounds Algorithm was used to create the second and third models, the second using \overline{R}^2 as a criterion for selection and the third using Mallows' C_p -statistic as a criterion for selection.

All three of these models did a very good job of predicting the old data as determined by the \mathbb{R}^2 value, however, in his final conclusion, prediction intervals were computed using the Omnitab computer package [20], and it was determined that both the Leaps and Bounds \mathbb{C}_p and the Leaps and Bounds \mathbb{R}^2 model did a better job of prediction than the SPSS model. Automatic Interaction Detection

It has been suggested that another method of prescreening variables prior to regression is the Automatic Interaction Detection (AID) computer package developed at the University of Michigan's Institute for Social Research and documented by Sonquist and Morgan [33,34]. This technique is primarily used in constructing models on sociological or categorical data and involves a single interval scaled criterion variable and a mixture of interval, ordinal, and nominally scaled predictor variables.

A typical problem in regression analysis is that one cannot always know in advance which transformations such as X_1^2 or $\ln(X_1)$, or interaction terms such as X_1X_1 to introduce in the model so that the predictive power of the model is maximized. A larger error term reported in much

of today's research may be partly due to the way in which these predictor variables are combined in the model, and it is this problem of locating specific interaction effects between variables, if in fact they do exist, that is the basis for this investigation. Since AID also determines the variables most important to the model, its main purpose in this investigation will be as a screening device to locate those variables most important to the regression model, thus reducing the number of possible variables considerably.

AID Algorithm and Objective

The AID analysis is somewhat of a branch and bound procedure using analysis of variance technique that is useful in studying the interrelationships among a set of variables and useful in maximizing the predictive power of a multiple regression model. Unlike most multiple regression procedures, linearity and additivity assumptions are not necessary requirements in the AID analysis.

The AID algorithm accomplishes a sequential division of the entire data into subsets based on that split which causes the greatest reduction in the unexplained variability of the criterion variable. On the first iteration, the entire data base is split into two groups around that variable which allows for the minimum within-group variability measured by the sum of squared deviations of the criterion variable from the group means. On each successive iteration, one of the existing groups is split in the same manner as in the first step. This process continues until one of the stopping criteria has been satisfied.

The AID model can be written as:

$$Y_{mi} = \mu_i + \epsilon_{mi}$$
 $m = 1, 2, ..., n$ $i = 1, 2, ..., g$ (34)

where: Y_{mi} is the m^{th} criterion variable observation in group i μ_{i} is the i^{th} group mean

 ε_{mi} is the random error of the m^{th} criterion variable observation in group 1

This random error term has the same assumptions as the random error term ϵ_1 which was discussed in Chapter II.

An estimate for μ_1 is \overline{Y}_1 , the sample mean of the observations in group i. Letting \overline{Y} be the sample mean for the criterion variable, the total variability in the criterion variable (in AID notation) can be stated as follows:

$$TSST = \sum_{\substack{i=1 \ m=1}}^{g} \sum_{m=1}^{n_i} (Y_{mi} - \bar{y})^2$$
 (35)

This value will be constant for any given set of n observations.

Equation (35) can be expanded to:

where: TSST is the total sum-of-squares for the entire sample

WSS is the within-group sum-of-squares

BSS is the between-group sum-of-squares

The last term can be simplified to:

$$BSS = \sum_{i=1}^{g} n_i (\bar{Y}_i - \bar{y})^2$$
(37)

The objective of the AID algorithm at each iterative step is to split the groups so that BSS is as large as possible thus making WSS

as small as possible. A good measure of the goodness of the resulting model is:

$$R^2 = BSS* TSST 0 \le R^2 \le 1$$
 (38)

where BSS* is the BSS of the existing groups. As in the multiple regression case, the \mathbb{R}^2 value indicates the fraction of the variability in the criterion variable explained by the regression equation. In AID, an \mathbb{R}^2 value close to one indicates that the splitting process has done a good job of grouping observations with nearly identical values of the criterion variable.

At each split, equation (34) can be written as:

$$TSS_{1} = WSS_{1} + BSS_{1}$$
 (39)

Using this notation, the AID algorithm at each iteration can be generalized as follows:

- (1) Select that unsplit sample group which has the largest total sum-of-squares around its own mean as a candidate for further splitting.
- (2) For each predictor variable, find the subset of observations in the group selected in Step 1 which maximizes BSS_i (or minimizes WSS_i).
- (3) Chose the best partition of observations on a predictor and split the group using that predictor variable.
- (4) Repeat Step 1 until a stopping criteria has been satisfied. The logic of the AID algorithm can be easily summarized in a flow diagram developed by Gooch [14] and simplified by McNichols [25] in Figure 2.

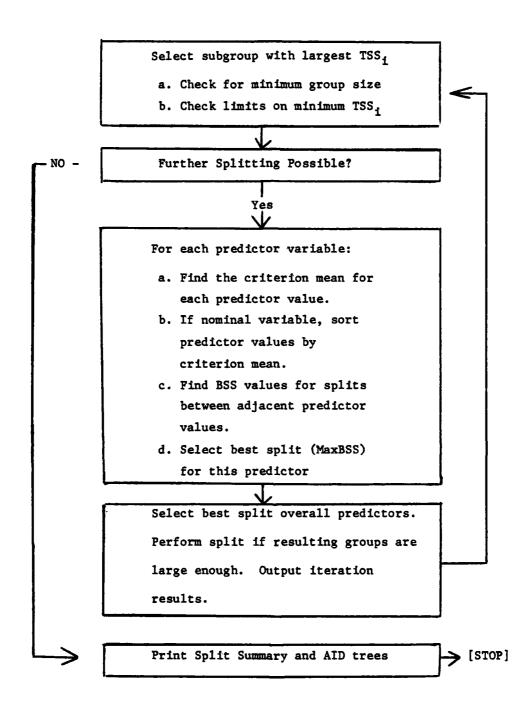


FIGURE 2 Logic of the AID Algorithm

Stopping Criteria

There are four important stopping criteria used in the AID algorithm which are indicated by the user.

- (1) The maximum number of final groups including those which can and cannot be further split cannot exceed the value MAXGP or termination will occur.
- (2) The number of observations in each group that is split cannot be less than the value NMIN.
- (3) The total sum of the squares in a group, TSS_1 , cannot be less than P1 percent of the total sum of squares for the entire sample, TSST. Numerically speaking, P1 < $TSS_1/TSST$.
- (4) Any split must reduce the original within group sum of squares by P2 percent or the AID algorithm is terminated.

 Gooch suggests that:

P1 > .01

P2 > .005

MAXGP < 90

NMIN \geq 5% of the total number of observations

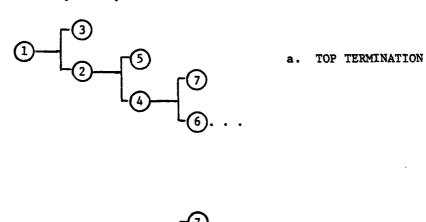
Analysis of the AID Output

One of the main features of the AID package is the three diagram which graphically describes the splitting process of each of the groups. The structure of these trees is very important in determining the nature of the variable interactions in the model.

Sonquist and Morgan describe two basic structures or shapes of the trees, the trunk-twig structure, and the trunk-branch structure.

The truck-twig structure allows only one of two groups split to be split again. The group that is not split is classified a final group.

There are three basic types of trunk-twig structured trees: top termination, bottom termination, and alternating termination (See Figure 3). The top termination structure is referred to by Sonquist as an "alternative advantage" model, where the nature of the advantage is determined by the characteristic which split the group. In this structure, those groups in the upper branches always have a higher mean value than the lower branches, and once formed, these upper branches cannot be split any further.



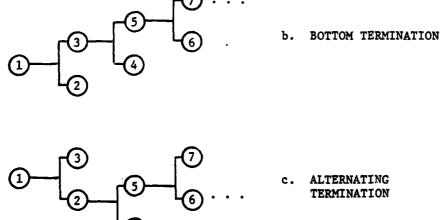


FIGURE 3 Trunk-Twig Structured AID Trees

Sonquist refers to the bottom-termination structured tree as an "alternative disadvantage" tree, where the nature of the disadvantage is determined by the characteristic which split the group. In this case, the lower branches once formed, cannot be split further.

In the alternating termination structure, the interpretation can be viewed as a combination of the two preceding structures whereby the importance of a split depends solely on the characteristics of the variable which split the group.

The trunk-branch structure is analogous to the trunk-twig structure except that each group split is a candidate for further splitting. This type of tree structure is typical of the first few splits in any AID tree. Once the first few splits on a group have been made, the structure usually exemplifies that of the trunk-twig structure.

Besides the structure of the tree, the symmetry of the tree, or lack thereof, concerning the extent to which the same variables appear in a split on various trunks is important also. Non-symmetry implies that an interaction exists. Also, if a variable is split on one trunk and shows no indication of reducing the predictive power in another trunk, then there is a clear evidence of an interaction effect between that variable and those used in the preceding splits. The predictive power of each variable in a group is evaluated by the statistic BSS₁/TSS₁ and is shown on the selected AID output in Appendix D. This statistic represents the proportion of the variation in the group to which the predictor variable is being applied that would be explained if that group were split.

Preparation for the use of AID

In order to use the AID computer package, several important steps had to be followed. First of all, the data had to be transformed so that an integer format could be used to describe each data element in a six place field. Since many variables were calculated to as many as 13 decimal places, those variables had to be multiplied or divided by a specified factor of 10 and then truncated. For example: LSC/OH was multiplied by 10⁴ then truncated, so LSC/OH(27) = 26.63122286176 became 266312.

It is possible that by reducing the number of significant places, round off errors and non-comparible values would result.

Secondly, all data points for each variable had to be sequentially ordered and placed into groups or categories of equal size. (See Table VIII) This is done so that when the groups are split by AID, each mean will be stable with respect to the elements in that group.

After the data is transformed to the proper form, the computer deck can be formed. The itemized input is described in Appendix C. Results

As stated earlier, the important parameters in the AID input are P1, P2, NMIN, and MAXGP. Many attempts with various combinations of these parameters were made and are described in Table IX.

In the first four runs NMIN was set to 4, which means that no groups will be split unless there are at least 8 data points in that group (4 for each subgroup split).

TABLE VIII Sequential Ordering of Variables

| Variable | No. | Recode |
|-----------------|-----|----------------------------------|
| FGTNAV | 1 | 0 LESS THAN 1 |
| | | 1 OR OVER |
| BOMNAV | 2 | 0 LESS THAN 1 |
| | | 1 1 OR OVER |
| CARNAV | 3 | 0 less than 1 |
| | | 1 1 OR OVER |
| FGTSEN | 4 | 0 LESS THAN 1 |
| | | 1 1 OR OVER |
| Bomsen | 5 | 0 less than 1 |
| | | 1 1 OR OVER |
| FGTCOM | 6 | 0 less than 1 |
| | | 1 1 OR OVER |
| вовсом | 7 | 0 less than 1 |
| | | 1 1 OR OVER |
| UNIT PRICE | 8 | 0 LT. OR EQ.TO 2241 |
| | į | 1 2242 TO 3914 2 3915 TO 8410 |
| | | 3 8411 TO 19274 |
| | | 19275 OR OVER |
| VOLUME | 9 | 0 LT. OR EQ. TO 275 |
| | | 1 276 TO 560 2 561 TO 1377 |
| | | 3 1378 TO 1734 |
| | | 4 1735 OR OVER |
| WEIGHT | 10 | 0 LT. OR EQ. TO 850 |
| | | 1 851 TO 1500 |
| | | 2 1501 TO 3600 |
| | | 3 3601 TO 4900 4 4901 OR OVER |
| · | | 4 4901 OR OVER |
| COMPONENT COUNT | 11 | 0 LT. OR EQ. TO 88 |
| | | 1 89 TO 399 |
| | | 2 400 TO 911 |
| | | 3 912 TO 1186 4 1187 OR OVER |

TABLE VIII (Cont'd)

| Variable | No. | Recode |
|----------------|-----|------------------------------|
| PERCENTDIGITAL | 12 | 0 LT. OR EQ. TO 50 |
| | } | 1 51 TO 440 |
| | | 2 441 TO 550 |
| | | 3 551 TO 870 |
| | | 4 871 OR OVER |
| PERCENTANALOG | 13 | 0 LT. OR EQ. TO 240 |
| |) | 1 241 TO 740 |
| | | 2 741 TO 750 |
| | | 3 751 TO 990 |
| | | 4 991 OR OVER |
| PERCENTEM | 14 | 0 LT. OR EQ. TO 5 |
| | | 1 6 TO 20 |
| | | 2 21 TO 140 |
| | | 3 141 TO 760 |
| | | 4 761 OR OVER |
| PERCENTPS | 15 | O LT. OR EQ. TO 5 |
| | | 1 6 TO 80 |
| | | 2 81 OR OVER |
| PERCENTXMTR | 16 | 0 LT. OR EQ. TO 100 |
| | | 1 101 TO 190 |
| | | 2 191 TO 250 |
| | | 3 251 OR OVER |
| PERCENTSS | 17 | 0 LT. OR EQ. TO 230 |
| | | 1 231 TO 860 |
| | | 2 861 TO 975 |
| | | 3 976 TO 995 |
| | | 4 996 OR OVER |
| POWERDIS | 18 | 0 LT. OR EQ. TO 60 |
| | | í 61 TO 150 |
| | | 2 151 TO 270 |
| | | 3 271 TO 500 |
| | | 4 501 OR OVER |
| BITFIT | 19 | 0 LT. OR EQ. TO 5 |
| | | 1 6 TO 40 |
| | | 2 41 TO 130 3 131 OR OVER |
| j | | 3 131 OR OVER |

TABLE VIII (Cont'd)

| Variable | No. | Recode |
|----------|-----|---|
| ıc | 20 | 0 LT. OR EQ. TO 1 1 2 TO 5 |
| | | 2 6 TO 77 3 78 OR OVER |
| SRU | 21 | 0 LT. OR EQ. TO 3 1 4 TO 9 2 10 TO 12 |
| | | 3 13 TO 16 4 17 OR OVER |
| QPA | 22 | 0 LESS THAN 2 1 2 OR OVER |

TABLE IX
Result of AID Runs

| | | | _ | Run Nur | nber | | | |
|----------------|------|------|-------|---------|------|------|----------|------|
| Parameters | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Pl | .015 | .01 | .0015 | .001 | .005 | .015 | .01 | .005 |
| P2 | .015 | .01 | .0015 | .001 | .005 | .005 | .005 | .005 |
| NMIN | 4 | 4 | 4 | 4 | 3 | 3 | 3 | 5 |
| MAXGP | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 |
| R ² | .617 | .617 | .683 | .683 | .694 | .689 | .694 | .596 |
| | | | | | | | | |
| Variables* | | | | | | | | |
| v | Х | х | х | х | х | Х | х | X |
| AN | х | х | х | х | х | х | х | X |
| w | х | x | x | х | х | х | х | х |
| сс | x | х | х | х | х | | х | х |
| CARNAV | х | х | х | х | х | х | х | |
| XMTR | | x | х | х | х | х | х | |
| PD | | | х | x | х | х | х | х |
| UP | | | | | | | | х |

^{*} Those which AID determined.

This value was lowered to 3 in the following 3 runs. Notice that when NMIN was increased to 5 in run number 8, R^2 decreased from .694 in run number 8 to .596. So indeed, these parameters are important in modeling decisions.

The two best runs (based on highest R² values) were runs 5 and 7, where number 7 contains three parameters recommended by Gooch. Run number 7 was chosen as the test case to build the regression model used in this research and two approaches were developed from this run. The AID tree and results for run number 7 are described in Figure 4 and Table X.

Since the main objective of using AID is to reduce the total number of variables used and only choose those which are most important to the regression, a choice can be made as to where to stop considering variables for analysis purposes.

If the analysis is stopped when N reaches 4, then three variables remain: V, W, and AN. Considering interaction terms or cross produce terms, six variables can be used: V, W, AN, V·W, V·AN, and W·AN.

Another choice would be to stop considering variables for analysis when N reaches 3. In this case, 7 variables remain, V, W, CC, PD, AN, XMTR and CARNAV. AN and XMTR can be considered partial indicators in the sense that they can be represented as indicators (0 or 1) where zero indicates that AN or XMTR equals zero and the value one indicates that AN or XMTR is greater than zero. These indicator variables are referred to in the analysis as IAN and IXMTR. CARNAV is a pure indicator (either 0 or 1). In this case it was decided to use interaction terms between the first six original variables and the

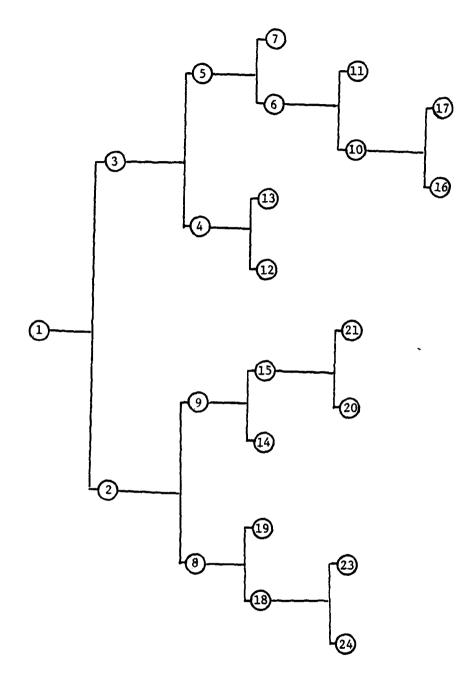


Figure 4 AID Tree for Run No. 7

TABLE X

AID Tree Results for Run No. 7

| GROUP | VARIABLE | RECODE | MEAN | STD. DEV. | N | R ² |
|-------|----------|--------|----------|-----------|----|----------------|
| 1 | _ [| | 13687.90 | 15871.88 | 63 | - |
| 2 | v | 0 1 2 | 6708.97 | 7352.77 | 38 | .294 |
| 3 | V | 3 4 | 24295.88 | 19133.53 | 25 | .294 |
| 4 | AN | 1 3 4 | 11667.33 | 9052.37 | 9 | .435 |
| 5 | AN | 0 2 | 31399.44 | 19640.68 | 16 | .435 |
| 6 | cc | 1 3 4 | 25506.08 | 9193.78 | 12 | .540 |
| 7 | сс | 0 2 | 49079.50 | 29540.98 | 4 | .540 |
| 8 | W | 0134 | 4040.72 | 4309.02 | 29 | .595 |
| 9 | W | 2 | 15306.67 | 8460.32 | 9 | .595 |
| 10 | CARNAV | 0 | 21670.25 | 9449.06 | 8 | .617 |
| 11 | CARNAV | 1 | 33177.75 | 4745.71 | 4 | .617 |
| 12 | cc | 2 4 | 6328.60 | 3030.33 | 5 | .638 |
| 13 | СС | 1 3 | 18340.75 | 9629.98 | 4. | .638 |
| 14 | AN | 3 4 | 6313.67 | 1385.32 | 3 | .661 |
| 15 | AN | 0 1 2 | 19803.17 | 6763.90 | 6 | .661 |
| 16 | PD | 4 | 17311.25 | 7900.37 | 4 | .670 |
| 17 | PD | 2 3 | 26029.25 | 6508.13 | 4 | .670 |
| 18 | XMTR | 0 1 | 2957.56 | 3052.07 | 25 | .684 |
| 19 | XMTR | 2 3 | 10810.50 | 4820.07 | 4 | .684 |
| 20 | PD | 1 4 | 16137.67 | 4832.67 | 3 | .689 |
| 21 | PD | 2 | 23468.67 | 6417.00 | 3 | .689 |
| 22 | W | 1 3 | 943.50 | 670.84 | 12 | .694 |
| 23 | W | 0 | 4816.69 | 3208.98 | 13 | .694 |

three indicators variables. A total of twenty-three variables are created in this case. A list of both sets of variables created in this case are listed in Table XI.

In order to decide which model should be used, each set of variables was run through the IMSL-RLEAP (Leaps and Bounds) program described earlier. Using \overline{R}^2 as a criterion, the 23-variable model explained 71.8 percent of the variance with 17 of the 23 variables, while the 6-variable models only explained 50.1 percent of the variance using all six variables. See Appendix D for a selected AID output and Appendix F for a selected Leaps and Bounds output.

Next a log transformation was made on the 23-variable model and run through Leaps and Bounds, and, surprisingly, the results did not show an improvement over those of the untransformed data. Thus, the untransformed 17 variables chosen by Leaps and Bounds were accepted as those AID determined most important. This model will therefore be used in the cross-validation experiments to follow. This 17-variable model is described in Table XII.

TABLE XI

Variables in the Two AID Models Considered

| Model 1 | Model 2 |
|---------|---------------|
| v | v |
| AN | w |
| W | сс |
| v·w | PD |
| V · AN | AN |
| W-AN | XMTR |
| | CARNAV |
| | V - CARNAV |
| | W·CARNAV |
| | CC · CARNAV |
| | PD - CARNAV |
| | XMTR · CARNAV |
| | V. IAN |
| | V·IXMTR |
| | W·IAN |
| | W·IXMTR |
| | CC · IAN |
| | CC · IXMTR |
| | PD·IAN |
| | PD.IXMTR |
| | AN.IXMTR |
| | XMTR · IAN |
| | IAN |
| | IXMTR |

TABLE XII

AID Regression Model Determined by Leaps and Bounds

| | LSC/OH = $B_0 + \sum_{i=1}^{17} B_i X_i$ | | | | | | | |
|----|--|----------------|-----------|--|--|--|--|--|
| | $R^2 = .718$ | | | | | | | |
| í | B ₁ | x _i | Partial-F | | | | | |
| 0 | 2.658290567 | - | - | | | | | |
| 1 | 155899×10^{-2} | v | 11.7804 | | | | | |
| 2 | 779107×10^{-1} | W | 22.7635 | | | | | |
| 3 | $.105464 \times 10^{-2}$ | PD | 5.52895 | | | | | |
| 4 | $.961796 \times 10^{-1}$ | XMTR | 8.75757 | | | | | |
| 5 | $.261128 \times 10^{1}$ | CARNAV | 7.58031 | | | | | |
| 6 | .700891 x 10 ⁻¹ | W. CARNAV | 14.4932 | | | | | |
| 7 | 506175 x 10 ⁻² | PD. CARNAV | 18.0098 | | | | | |
| 8 | 267022×10^{-1} | AN•CARNAV | 7.62132 | | | | | |
| 9 | .878194 x 10-3 | V.IAN | 9.5718 | | | | | |
| 10 | 12007 x 10-2 | w•IAN | 17.8296 | | | | | |
| 11 | $.143445 \times 10^{-2}$ | W·IXMTR | 3.85888 | | | | | |
| 12 | $.204243 \times 10^{-2}$ | CC-IAN | 12.2973 | | | | | |
| 13 | 112446 | CC.IXMTR | 13.4675 | | | | | |
| 14 | $.21432 \times 10^{-2}$ | PD.IAN | 15.1695 | | | | | |
| 15 | 402166×10^{-2} | PD.IXMTR | 22.0968 | | | | | |
| 16 | .153848 | XMTR.IAN | 8.40514 | | | | | |
| 17 | 547619 × 10 ¹ | IXMTR | 7.77109 | | | | | |

V Cross Validation, Conclusions and Recommendations Cross Validation

Three equations developed by Pulcher and one developed by Westinghouse have been reviewed, and one model developed by AID has been analyzed. All have been based on the old Westinghouse data collected in Phase I containing 63 data points.

A cross validation procedure was used to determine how well these old models predict the new 71 data points contained in the Phase II.

The first step was to use the new data in each of the old models to find the cross validation SSE and SST. They were then used to find the cross validation \mathbb{R}^2 described in Chapter II. A summary of results is given in Table XIII.

In both the Westinghouse model and the AID model, the cross validation SSE was greater than the SST. This would tend to imply that neither of the two models predict the new data very well. This is a surprising result especially for the Westinghouse model.

One possible explanation for this is that the Westinghouse model was developed in such a way that much of the idiosyncrecies of the data were explained. Notice the vast difference between the first model described in Table IV and the second described in Table V. This could also be the reason why the AID model failed to predict the new data.

TABLE XIII

Cross Validation Results

| Model | c.v. SSE | SST | c.v. R ² |
|------------------------|----------------|--------------|---------------------|
| L & B - R ² | 157.9096802275 | 227.701363 | .3065053361 |
| L&В-С _р | 112.4418454273 | 227.701363 | .50618720 |
| SPSS | 89.457779054 | 227,701363 | .6071269467 |
| Westinghouse | * | 227.701363 | * |
| AID | * | 1755.2523798 | * |

^{*} c.v.SSE was greater than SST

The best model determined by the cross validation criterion was Pulcher's SPSS model which had a c.v. R² value of .607 (see Table XIII). Using those variables, updated coefficients have been computed (see Table XIV). This new model using the old variables and just the Phase II data has an R² value of .780 indicating that 78% of the variance in the dependent variable is explained by the model. With the complete set of data (134 data points) 70.9% of the variance was explained by the model. Table XV describes this model. (See Appendix E for selected outputs from SPSS.)

Conclusions

A review of past research indicates that much literature is available on criterion in the selection of variables in a multiple regression thus indicating that it is an important subject not only for mathematicians or operations researchers, but is important to anyone attempting to develop valid models both for description and prediction purposes. As a result, these criteria give the statisticians a useful index of how well various models fit the data, however, experience shows that the result of using a single criterion should not be accepted as a final answer, but should be used with other available statistics and individual's intuitive judgement in developing a sound analysis.

This cross validation \mathbb{R}^2 value was useful in evaluating the prediction capabilities of the five models discussed. The three models which used log transformed data and were developed by Pulcher for description purposes on the old Westinghouse data

TABLE XIV

Pulcher's SPSS Model fitted to the New Data Points

| $ \ln LSC/OH = \alpha_0 + \sum_{i} \alpha_i D_i + \sum_{j} \beta_{j0} \ln x_j + \sum_{i} \sum_{j} \beta_{ji} D_i \ln x_j \\ i \qquad j \qquad \qquad j \qquad i $ | | | | |
|---|------------------|-------------|--|--|
| $\bar{R}^2 = .67923$ | $R^2 = .78004$ | F = 7.73752 | | |
| Variable Name | Coefficient | Partial-F | | |
| UP | .36000615 | .17946696 | | |
| w | .60315963 | .43885436 | | |
| SS | 1102.0708 | 280.30031 | | |
| NB | 8.2056618 | 17.346404 | | |
| SF | 33287310 | .39887747 | | |
| SB | .99001459 | .83450842 | | |
| DIG | -1.3736140 | 2.5219780 | | |
| EM | 2.6000225 | 1.6961873 | | |
| PS | .12680075 | .31751393 | | |
| NF * UP | .13008302 | .15751183 | | |
| NF * CC | 13099197 | .22804494 | | |
| NB * UP | 34773058 | 1.1390687 | | |
| NB * V | - | _ | | |
| NB * W | 75005236 | 2.6271934 | | |
| DIG * V | 14280299 | .60250900 | | |
| DIG * W | .49276704 | .61187387 | | |
| AN * UP | .06467638 | .13817898 | | |
| AN * W | 13646127 | .43869986 | | |
| EM * V | 35382193 | .25552978 | | |
| XMTR * CC | 36370529 | .46191312 | | |
| XMTR * SS | 531.35247 | 667.96390 | | |
| BF * W | .0559571 | .2229430 | | |
| BF * SS | 59.533507 | 207.10304 | | |
| Constant | -10.43849 1.4928 | | | |

^{**}Removed from the equation by SPSS.

TABLE XV

Pulcher's SPSS Model Variables fitted to the Entire Data Set

(Phase I & Phase II)

| (Phase I & Phase II) $\ln LSC/OH = \alpha_0 + \sum_{i} \alpha_i D_i + \sum_{j} \beta_{j0} \ln x_j + \sum_{j} \sum_{i} \beta_{ji} D_i \ln x_j$ | | | | |
|---|-------------|------------|--|--|
| | | | | |
| Variable Name | Coefficient | Partial-F | | |
| UP | 7.1760834 | 2.6076596 | | |
| w | - ,58168533 | 2.8060750 | | |
| SS | 31049321 | .45804725 | | |
| NB | 12129190 | .00539864 | | |
| SF | -1.0966765 | .78704103 | | |
| SB | .20884626 | .69860270 | | |
| DIG | .16839348 | 3.1550771 | | |
| EM | .50533178 | 16.807697 | | |
| PS | .43488570 | 2.1115964 | | |
| NF * UP | .036039607 | .13695163 | | |
| NF * CC | 048746736 | .11610925 | | |
| NB * UP | 11413454 | .22280423 | | |
| NB * V | -1.7249398 | 2.2502326 | | |
| NB * W | 2.17249398 | 2.2513077 | | |
| DIG * V | 19976096 | .23782540 | | |
| DIG * W | .32683368 | .50702946 | | |
| AN * UP | .024885722 | .0627402 | | |
| an * w | .032724716 | .012309140 | | |
| EM * V | .14565893 | .59932259 | | |
| XMTR * CC | .29069072 | 7.6961250 | | |
| XMTR * SS | 38171889 | 5.9613262 | | |
| BF * W | .028545024 | .31109000 | | |
| BF * SS | 008700618 | .0471961 | | |
| Constant | 70977903 | 85.146786 | | |

had adequate predictive capabilities; the other two models (the Westinghouse model and the AID model) were determined not to have very good predictive capabilities.

The Automatic Interaction Detection Algorithm was useful in prescreening important variables and reducing the total number of variables to be used in a multiple regression, however, it did not prove to be the best technique in developing regression models, for the maximum \mathbb{R}^2 value was only .780.

Recommendations

In his research, Pulcher used the Chow Test as a screening device to determine the most important variable subset using a Product of Powers model. However, one assumption in using the test is that of equal variances on the error term. In future analysis, I would recommend the use of a technique developed by Jayatissa [21] of Tests of Equality Between Subsets of Coefficients in Two Multiple Regressions assuming unequal variances. This can be used as a prescreening device to locate important variables. Then stepwise regression procedures using SPSS can be used to develop a multiple regression model.

To the personnel at the Avionics Laboratory, I would recommend that cross validation studies be made to insure that models developed by contractors be able to predict new data so that new models do not have to be developed every time new data is obtained.

All techniques used on this analysis were based on minimizing the sum of squared errors. The many criterion for selection of variables mentioned in this report should be given further consideration.

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APPENDIX A

LRU DESCRIPTION

APPENDIX A

| No. | LRU-ID | AIRCRAFT | DESCRIPTION |
|-----|--------|----------|-------------------------------|
| 1 | 71B2Ø | F4E | Amplifier, Computer |
| 2 | 7353Ø | F4E | Ballistics, Computer |
| 3 | 71LBØ | F4E | Receiver-Transmitter |
| 4 | 71HKØ | F4E | Platform, Gyro, Stab. |
| 5 | 71PKØ | RF4C | Receiver-Transmitter |
| 6 | 71PBØ | RF4C | Amplifier, P.S. RCVR |
| 7 | 71710 | RF4C | P.S. Leveling, Amplifier |
| 8 | 724GØ | RF4C | Power Supply |
| 9 | 71G5Ø | RF4C | Computer, Navigation |
| 10 | 71FAØ | F15A | Amplifier, Electronic |
| 11 | 71FBØ | F15A | Gyroscope, Displacement |
| 12 | 71CAØ | KC135A | Receiver-Transmitter |
| 13 | 71DAØ | F15A | Receiver-Transmitter |
| 14 | 71ABE | в52н | Receiver |
| 15 | 71ADA | в52н | Receiver-Transmitter |
| 16 | 73DBA | в52н | Receiver-Transmitter |
| 17 | 71ACC | в52н | Receiver |
| 18 | 73CBØ | в52н | Amplifier |
| 19 | 73CEN | В52Н | Computer, A2 and EL |
| 20 | 73CFK | B52H | Receiver-Transmitter |
| 21 | 73DAH | в52н | Amplifier, Electronic Control |
| 22 | 73EBA | в52н | Amp, Astrotrack, Servo |
| 23 | 73EBF | В52Н | Signal Amplifier |
| *24 | 71CAØ | F15A | Receiver |
| 25 | 72EAA | KC135A | Receiver-Transmitter |
| 26 | 72ECA | KC135A | Amplifier, Electronic Control |
| 27 | 72BP0 | C5A | Measurement Unit, IMU |
| 28 | 71JAØ | C5A | Receiver, VHF Navigational |
| 29 | 71LAØ | C5A | Receiver-Transmitter |
| 30 | 72DNØ | C5A | Processor Data |

^{*} DUPLICATE LRU-ID -- Placed on a Different Aircraft

APPENDIX A

LRU Description (Con't)

| No. | LRU-ID | AIRCRAFT | DESCRIPTION |
|-----|--------|----------|-------------------------------|
| 31 | 72ACØ | C5A | P.S., Thermal Control |
| 32 | 7171A | C130E | Receiver |
| 33 | 7131D | C130E | Receiver-Transmitter |
| 34 | 72RFØ | C130E | P.S. Power Supply |
| 35 | 72RBØ | C130E | Amplifier |
| 36 | 51eaø | F15A | Computer, Air Data |
| 37 | 52AAØ | F15A | Computer, Flight Control |
| 38 | 52ABØ | F15A | Computer, Flight Control |
| 39 | 63BDØ | F15A | Control Panel, Int Nav |
| 40 | 71AEØ | F15A | Inertial Measurement Unit |
| 41 | 71AKØ | F15A | Control Indicator, Nav |
| 42 | 74JAØ | F15A | Indicator, Multiple Air Nav |
| 43 | 74ЈСØ | F15A | Processor, Signal Data |
| 44 | 52GA1 | F106 | Amplifier-Interface |
| 45 | 71JCE | C5A | Control Panel VHF Nav |
| 46 | 72AEØ | C5A | Computer-Primary, IDNE |
| 47 | 72CCØ | C5A | Computer-Analog/Digital |
| 48 | 712AØ | C130E | Receiver-Transmitter |
| 49 | 71ZBØ | C130E | Digital/Analog Converter |
| 50 | 71ZDØ | C130E | Control Unit |
| *51 | 71ZAØ | F111D | Receiver-Transmitter |
| *52 | 71ZBØ | F111D | Digital/Analog Converter |
| 53 | 712CØ | F111D | Control |
| 54 | 73EGØ | F111D | Computer, General Purpose |
| 55 | 73EPØ | F111D | Converter-Multiplexer |
| 56 | 73HAØ | f111D | Stabilizer Platform |
| 57 | 73HCØ | F111D | Navigational Computer |
| 58 | 73NAØ | F111D | Indicator, Horizontal Display |
| 59 | 73NBØ | F111D | Processor, Horizontal Display |
| 60 | 73QBØ | F111D | Electronic Unit, Radar |

^{*} DUPLICATE LRU-ID -- Placed on a Different Aircraft

APPENDIX A

LRU Description (Con't)

| No. | LRU-ID | AIRCRAFT | DESCRIPTION |
|-----|---------------|----------|------------------------------|
| 61 | 73SC0 | F111D | Indicator, Digital Display |
| 62 | 73KBØ | F111D | Antenna-Receiver |
| 63 | 73KEØ | F111D | Amplifier, Power Supply |
| 64 | 73KFØ | F111D | Synchronizer-Transmitter |
| 65 | 73DDØ | F111D | Computer, Terrain Following |
| *66 | 71CAØ | FB111A | Receiver Unit |
| 67 | 73EGØ | FB111A | Computer, General Purpose |
| 68 | 73HCØ | FB111A | Navigational Computer Unit |
| 69 | 73LAØ | FB111A | Electronic Unit |
| 70 | 7593Ø | F4E | Weapons Release Control |
| 71 | 74BD Ø | F4E | Computer |
| 72 | 74BF Ø | F4E | Transmitter |
| 73 | 7481Ø | F4E | Gyroscope, Lead Comp. |
| 74 | 76A1Ø | RF4C | Analyzer, Pulse |
| 75 | 76GAØ | RF4C | Signal Processor |
| 76 | 74F FØ | F15A | Processor |
| 77 | 74 FAØ | F15A | Transmitter |
| 78 | 74FHØ | F15A | Power Supply |
| 79 | 74FUØ | F15A | Antenna |
| 80 | 77ECØ | в52Н | Flir Signal Proc. |
| 81 | 77EEØ | в52Н | Flir Turret Drive |
| 82 | 77DCA | в52н | STV Camera, Electronic |
| 83 | 77DBØ | в52Н | STV Turret Drive |
| 84 | 73CRØ | F4E | Laser Control, Electronic |
| 85 | 73CG Ø | F4E | Two Axis Gimbal Assembly |
| 86 | 65BHØ | F15A | Processor, Radar Target Data |
| 87 | 74FC Ø | F15A | Receiver, Radar |
| 88 | 74 FJØ | F15A | Oscillator-RF |
| 89 | 74FKØ | F15A | Radar Set Control |
| 90 | 74FQØ | F15A | Processor, Radar Data |

^{*} DUPLICATE LRU-ID -- Placed on a Different Aircraft

APPENDIX A
LRU Description (Con't)

| No. | LRU-ID | AIRCRAFT | DESCRIPTION |
|-----|--------|----------|---------------------------|
| 91 | 74KAØ | F15A | Display Unit, Head Up |
| 92 | 74KCØ | F15A | Processor Signal Data |
| 93 | 75AEØ | F15A | Converter-Programmer |
| 94 | 74CAØ | F4E | Indicator, Control |
| 95 | 74CBØ | F4E | Indicator, Pilot |
| 96 | 74CCØ | F4E | Indicator, PSO, IO |
| 97 | 74FA1 | F106 | _ |
| 98 | 74EBØ | F15A | Lead Computing Gyro |
| 99 | 76AEA | В52Н | Transmitter |
| 100 | 73KAØ | FB111A | Computer, TFR |
| 101 | 73PHØ | F111D | Power Supply, LV |
| 102 | 73PBØ | F111D | Processor, Electronic |
| 103 | 73PDØ | F111D | Radar Transmitter |
| 104 | 73PFØ | F111D | Signal Data Converter |
| 105 | 73РМØ | F111D | Reference Signal Gen. |
| 106 | 71NA0 | F4E | Receiver-Transmitter |
| 107 | 71QUØ | RF4C | Receiver-Transmitter |
| 108 | 63AAØ | F15A | Receiver-Transmitter |
| 109 | 65AA0 | F15A | Receiver-Transmitter |
| 110 | 63BAA | В52Н | Receiver-Transmitter |
| 111 | 63CAA | В52Н | Receiver-Transmitter |
| 112 | 65BAA | В52Н | Receiver-Transmitter |
| 113 | 61BBA | B52H | Receiver |
| 114 | 65BAA | KC135A | Receiver-Transmitter |
| 115 | 63AF0 | KC135A | Receiver-Transmitter |
| 116 | 63AA0 | C5A | Receiver-Transmitter |
| 117 | 63121 | C130E | Receiver-Transmitter |
| 118 | 63AAA | C130E | Receiver-Transmitter |
| 119 | 55ALØ | C5A | Central Multiplex Adapter |
| 120 | 55AVØ | C5A | Computer Digital, Madar |

APPENDIX A

LRU Description (Con't)

| No. | LRU-ID | AIRCRAFT | DESCRIPTION |
|------|---------------|----------|----------------------------|
| 121 | 61AAØ | C5A | Exciter Receiver, HF/SSB |
| 122 | c1ACØ | C5A | Amplifier/Antenna Coupler |
| 123 | 61AEØ | C5A | Panel, Control, HF/SSB |
| 124 | 62AAØ | C5A | Transceiver, VHF Comm |
| 125 | 63A6Ø | F15A | Radio Receiver |
| 126 | 63BCØ | F15A | Control Panel, Int Comm |
| 127 | 63BF Ø | F15A | Control Panel, IFF |
| *120 | 61AAØ | FB111A | Receiver-Transmitter |
| 129 | 61ABØ | FB111A | Amplifier-Power Supply |
| *130 | 61ACØ | FB111A | Control |
| 131 | 72AAØ | FB111A | Control, Radar Transponder |
| 132 | 72ACØ | FB111A | Receiver Transmitter |
| 133 | 64211 | C130E | Intercom Set |
| 134 | 64212 | C130E | Control Panel |

^{*} DUPLICATE LRU-ID -- Placed on a Different Aircraft

APPENDIX B: PART 1

LISTING OF PHASE I DATA

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N LRU-ID BOMBER CARGO SENSORY COMM

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APPENDIX B: PART 2

LISTING OF PHASE II DATA

N LRU-IN BOMBER CARGO SENSORY COMMUP V N CC DIG AN EM FO XMTF SS PO BITFIT IC SEU QFA LSC/UH UF 11 71F80 N. 6. · 13.90 61. 421 . 11308. 0.0 0.0 1. 2.809/530526538 33.u 67. ii B .i. 17.i 1. 33. 1 175. 1. 2.38 27 7 29 PO C. 0. 75.Ch +203. ₽. • 1. 253330. 2+75. 30.0 1.6 0.1 59.0 1. 26.5312228517591 737. 93.6 371. 24. 4. . 1.29 36 51EA0 5. 0. C. 16.30 1031. J. 15348. 542. 87.0 6.9 5.5 i.5 131. 14. 113. J 29.0 411 • 1. .5406343738969 2.37 ŋ. 37 5 2AA3 i e ٠. 15539. 11.80 1543. 1.6 4.5 65. 7. 668. ą6 .4 [• J 215. 100.0 0.0 1. .933+67°376722 2.39 0. 36 5 2A 90 11.66 11:2. (. 5 . P . 35115. 120.0 L.0 183.0 131. 44.5 125 . 12. 1. 1.0125826841586 2.3. 39 6 3805 r. *I*. • 2.00 73. 78. 2314. 0.0 180.0 0.1 Ş •^ 100.5 3. 7. 2.6 1. .5020535231998 0. 0. 80.00 3193. 1.5 5.; 2.30 40 71AE3 · . 1215. 1799. 35.7 7.1 7.1 192215. r . C 98.5 2+3. 1. 21.7335232505010 2.30 41 71AKE 8.65 453. . . 13557. 3:03. 37.4 2.t :. i • 3 37.4 55. 21. 191 . 9. 1.0168731737378 2.33 42 74JAC J. 21.50 253. 6.0 36.6 39. 16. 8033. 23579. 7.0 03.4 98.7 75. 54.1 1. 3.3712737356643 2.30 4. 43 74JCu 21.60 182... 25330. 1370. 48.5 i. • 8 U . 5 4 . 7 140.4 1032. J. (465. 16. .4137375911296 1. 2.30

```
N LRU-IN BOMBER CARGO SENSORY COMM
        DIG AN EH PS XMTH
SS PD BITFIT IC SMU QPA LSC/UH
UF
 44 5 2GA1
            η.
                  1. C. U.
        3+31. 235. 7.00 275.
+7.0 57.0 5.0 5.0 7.0 1.0
     100.0
                                                     .63 Fd 32G 35 29 18
     3.13
         7325. 31. 2.16 25.

0.0 50.0 50.0 50.0 1.7
 45 71JGE
                                              · . 0
     ÷ 1.0
                                            2.0
                                                   ·1+697663689uG
       .20

EJ 0. 1. 0. 0.

80345. 2267. 58.01 4275.

100.6 6.J 0.0 0.7 0.0

777 6.J 1174.0 93.0 1.0 2.3*69342645327
     1.20
 46 72AEJ
    187.3
     1.20
47 7 2000 n.
                  1.
                      0.
       27391. 1097. 26.00 1289.
70.0 31.0 0.0 0.0
          70.0 31.0 0.0 0.1
85. J.J 270.0 37.)
                                             · 0
    139.6
                                          1.0
                                                   +9450332555831
     1.20
22.0
                                            1.0
                                                   •1389+87303898
        7
6. 8. C. C.
1538. 154. 5.40 669.
50.4 50.4 C. 85.4
49 71783
                                 € • ប្
                                           F. D
    100.7
           25.
                  ្ត្
                            85.U
                                    1 • d
                                           1.9
                                                   .9373346352798
    2.33
         7. 1. 0. 0.

515. 34. 2.00 9.

7.0 1Ju.0 (.0 J.)

10. 0.3 17.0 1.0
50 71200
                                           • 0
1 • u
                                    1.6
                                                    .0107370435367
    1.23
        75.0 746. 20.56 2063.
75.0 7.6 L.0 3.0
51 717Au
                         اول الموا
                                           2 ° · U
    93.3
                                   1. î
                                            1.0
                                                   • 33 ?h 32 3u 7E 923
    2.33
52 7179G
       : • 0
    190.0
                                            1.0
                                                   • 73 9 3 1 6 7 2 2 4 0 8 0
    2.39
        515. 94. 2.EQ
0.0 100.0 0.0
53 71ZC0
                                 9+.
                           17.1 1.7
                                           r . c
   190.9
          10.
                  ນ້ອນ
                                           1.8
                                                    . 65 96 31 93 065 56
   2.33
```

```
N LRU-ID BOMBER CARGO SENSORY COMM
      UP V W CC
DIG AN EM PS XHTF
SS PO BITFIT IC SEU QPA LSC/OH
UF
1.30
    3EPJ r. J. C. U.
215330. 1435. 40.05 5015.
30.0 20.J 0.5 0.6 r.0
10J.0 460. 1.0 1926.0 69.3 1.0 5.3140.58227425
 5F 7 3EP)
     2.33
      56 / 3H49 C.
     2.30
     HC3 1. 3. F. C. 1. 121.11. 1327. 26.00 3027. 19.3 19.0 120. 2.0 713.0 22.6
 57 7 3HC3
                                        6.3
                                        1.0 2.8338628762542
    190.0
     1.37
 ~ · U
                                      1.] 2.9+953(2575585
     2.30
     3N36 0. 0. 0. 0. 3.

77239. 467. 14.00 1813.

35.0 14.0 1.0 0. .0

100.9 135. 0.3 543.0 17.7 1.0
 59 73N3L
                                               . 2350588898321
     2.30
 60 7 30 30 1.
      030 1. 6. 6. 6.
145751. 559. 20.00 662.
0.0 31.6 6.7 26.7
30.0 128. 1.J 9.0 11.7
                                         ^ • ü
                                        1.3 4.4339464932943
     139.9
     2.30
      61 7 3SC0
                                         ~ • U
                  10.0 0.3 0.5
0.0 611.0 17.5
                                        1.0 2.73 # 20 4 0 1 3 3 7 7 9
            66.
     144.0
     2.33
      62 73KBU
                                        · . 0
                                        2.0 2.7155518394649
                          u.5 12.1
            23ú.
                  ال و ب
      93.5
      2.30
      KEU f. 8. 0. 0. 6. 643.
 63 73KEU
           n.u (.) 6.2 31.º
                                        1.3
                                        2.0 .8377326421405
                           9.5 11.0
              9.
                    ن د ند
      31.8
     2.30
```

```
N LRU-ID ROMBER CARGO SENSORY COMM
          DIG AN EM PS XMTR
SS PO BITFIT IC SKU OFA LSC/OH
 UF
              18n. 82f. 27.6L 272.

0.0 97.2 2.8 L. 3.0

920. 2.0 0.0 3.1 2.0
  64 73KF0
           538n.
        95.8
                                                                .6378361204613
        2.30
    2.30
73KKJ 9. 8. [. L.
2507. 622. 16.46 315+.
9.0 19(.5 6.3 0.0
190.0 106. 3.0 7.3 14.9
  65 73KKJ
                                                      ( • i)
                                                       2.0
                                                                2.2393565>51848
       2.37
         Gu 1. J. L. C.
87249. 1573. 17.40 3322.
93.6 7.u 6.u 0.
  67 73EGu
                                          G . it
                                                       F . 0
       100.0
               225.
                       0.0 1543.0 21.0
                                                       2.9 8.1766395092129
       1.30
        103 1. J. C. 0.
121+11. 1327. 26.0u 3927.
41.7 39.0 19.3 0.6
 68 7 3HC0
                                                      ٠ . ن
      100.0
                                                       1.0 14.3548519875340
      1.30
3LAG 1. 5. 0. 6.
31554. 1272. 36.65 2982.
0.0 100.0 0.6 5.
       1.30
 69 73LAS
                                                   7.0
1.0 13.8516371801320
       1.30
            1. (. 1. ().
335. 222. 5.50 9.
0.0 ..0 106... 0.6 (.0
100. J.0 0.0 3.7 1.0
 81 77EEJ
        3 - 5
                                                       1 o ti
                                                               .0149339993166
       1.33
            0. 0. 1. 0.
2076. 750. 10.05 1308.
95.9 0.0 1.3 2.5
 86 55BH3
         2375.
                                                   • 6
       98.7
                                            7.0
                                                      1.0
                                                                . 4535356982371
       2.37
 87 74FC0 5.
     4FC0 5. 0. 1. C.
125433. 1173. 25.70 965.
0.0 100.) 9.0 0.6
100.0 300. 63.0 39.0 5.
                                                    5.0
     100.0
                                                      1.0
                                                            3.7433311998746
      2.30
        Jn 0. 9. 1. 1. 32377. 1723. 26.20 1073. 0.0 91.3 6.7 0.0 5.0
 88 74FJF
                                                  r.j
1.8
      91.3
                                                            3.4393592035185
      2.33
             e •
                   7. 1. 0.
119. 3.31 24.
6.9 10.5 3.3
. 0.0 8.0 1
84 74FK4
          4727.
                                  8.0
            30.0
                                           1.F 1.J .755634417COLD
      93.3
              20.
      2.33
```

```
N LRU-ID BOMBER CARGO SENSORY COMM
UP V N CC
         DIG AN EM PS XMTR
SS PO BITFIT IC SEU OPA LSC/OH
UF
90 74F00 0. 0. 1. 0.
120)95. 1747. 160.00 8293.
36.9 3.1 0.0 0.0 0.0
130.0 537. 56.0 2392.0 31.0 1.0 7.9795675759528
         Au n. u. 1. 6.
56)37. 2325. 38.60 522.
0.4 33.9 6.0 6.1 7.0
0.7 177. 36.0 181.0 19.7 1.0 1.819)320u13107
 91 74KAU
       23.7
      2.39
 92 74KC0
                      û. 1.
                                      ہ نا
              99. 592. 16.00 1755.
32.2 17.5 6.7 .3 f.0
136. J.0 1375.0 18.0 1.0 1.0367230884290
       36399. 592.
32.2 17.5
     130.0
      2.30
       AEO 0. 0. 1. 0.

34313. 1325. 37.00 +745.

90.5 5.9 3.0 0.0 0.0 0.0

97.0 58. 0.0 334.0 25.0 1.0 .0886397513855
93 75AE0
      97.0
      2.30
        AG G. 0. 1. 6.
19352. 1458. 36.66 2242.
35.6 13.2 1.2 G.C C.O
8.8 517. 0.0 29.0 29.0 1.J .1379087423807
               G.
94 74CAG
      98.8
      2.30
              0. 3. 1.
95 74CB0
          22/70. 1+76. 44.0. 813.
98.9 0.3 1.1 0.6 0.0
9 181. 3.7 38.0 17.0 1.0 .272715619760
      98.9
      2.35
       96 /4CCG
                                                        C. B
      99.4
                                                        1.0 .15/6510927325
      2.39
        A1 0. C. 1. C.
22335. 2761. 54.0C 4193.
99.8 C.U .2 U.C
97 74FA1
                                                       · . G
      39.8
              124. 23.0 869.0 101.0
                                                      1.0
                                                                 1.92433970931.9
      3.10
98 74ERO ..
             0. 0. 1. 0.
137. 951. 19.60 1773.
81.6 11.8 .7 6.0
135. 0.0 345.0 17.0
         37137.
                                                    ..0
      99.3
                                                       1.0 .9069222338535
      2.30
       1. C. 1. C. 2375.
42) 70. 2666. 92.60 2375.
C.O 0.0 6.0 0.0 100.0
13.9 1300. 11.7 105.0 13.9 1.0 13.758 953 67655 90
99 76AEA
      99.9
      . 30
```

```
N LRU-ID BOMBER CANGO SENSORY COMMUD V W CC
 DIG AN EM PS XMTP
SS PD BITFIT 1C SEU QPA LSC/OH
 UF
 108 73KAD 1.
            1. d. 1. d.
191. 622. 16. [u 3241.
1.0 95.8 1.2 u.h 7.0
200. 10.0 3.0 13.0 2.0 4.5583/32/24246
        10231.
      1.30
     31518. 952. 32.LU 1051.
 101 7 3PH9
                            6.5 100.0 i.0
4.0 12.5 2.0 1.4339743589744
     100.0
             465. 3.3
      1.29
      102 73PB(
     100.3
     1.20
103 73PD9
                  0.
                        1.
      139554. 4372. 145.00 723.
           0.0 0.0 0.0 0.0 107.0
3000. 7.0 2.0 7.0 1.0 10.5356957521370
     198.0
     1.20
104 7 3PF)
     3PF) n. u. 1. b. 254550. 2352. 51.00 2452. 88.2 11.8 0.0 0.0 7.0 1.0 1.1340364192564
     130.0
     3PMG 0. 0. 1. 1. 1. 49533. 1445. 33.01 707. 20.0 66.5 13.4 0.1 7.0 85.1 145. 0.0 4.0 8.4 1.0
105 7 3PMC
                                                 2.6533112020513
119 55ALu
       38]48. 1587. 46.60 381.

58.7 11.9 0.0 19.0 1.0

0.0 290. 44.0 290.0 2].0 1.0 1.7527+93316603
    100.0
     1.20
     103886. 1549. 30.85 725.
75.4 0.0 0.7 26
           0.
124 55AV9
                0.0 0.1 24.6 f.0
15.0 192.0 64. 1.0 1.0796582431369
           300.
    150.2
     1.20
      121 61AAû
    170.0
     1.39
     122 51AC9
                                         (.u
2.u 1.5227537260350
     53.6
     1.33
```

```
N LKU-ID BOMBER CARGO SENSORY COMM
            UP V W CC
            DIG AN EM PS XMIR
   SS PD BITFIT IC SRU QPA LSC/OH
   UF
   123 61AEJ 0. 1. 0. 1.
6358. 135. 4.30 471.
0.0 10:.0 6.0 6.0
100.3 70. 0.0 33.0 7.9 2.0 .3344129138392
         1.20
                       1. 6. 1.
364. 15.96 1116.
75.0 9.0 6.0
                  ŋ.
   124 6 2AAB
            3175.
                9 - 6
                                                       5r.0
         100.0
                  263. 0.0
                                      U . 5
                                             15.9 2.0
                                                                   .53273+4115429
         1.20
             7379. 428. 16.30 585.
59.1 38.2 2.7 0.3
3 32. 0.0 31.0 7.0
   125 5 3AGV
                                                      *•0
1•0
          97.3
                                                                   .4726744365490
          2.30
                        7. 0. 1.
267. 12.00 742.
7.0 0.0 39.3 7.0
0.0 73.0 12.0 1.0
                 9.
   126 63BC0
             1375.
                53.1
                  34.
         100.0
                                                                   .9372355726628
         2.30
                0. 0. 0. 1.
357. 78. 2.00 153.
38.7 0.0 0.0 11.3 (.3
3. 0.0 14.0 4.3 1.0
   127 538F0
             2357.
         100.0
                                                                   .0.1914153(564
           .30
A0 i. u. u. i. 1.
30591. 378. 13.12 195.
0.0 75.0 (.0 u.) 25.0
- 4562 0.0 7.u 13.0 1.0 2.9196024157021
         2.30
   126 61AA3
         190.0
         1.30
           90 1. 9. 0. 1.
14526. 598. 23.13 432.
0.0 43.8 32.0 24.2
4.0 150. 0.0 3.0 13.6
   129 61AB0
                                                       1.0
         139.3
                                                        1.0 2.7404372J25860
         1.39
         1ACO 1. U. L. 1.
12357. 132. 4.17 471.
0.0 10C.0 C.C C.
100.0 70. 11.7 33.0 6
   139 61AC0
                                             6 • C
                                                          . 0
         199.9
                                                        1.0 1.3/(2)44055592
         1.30
               1. 0. (. 1.
556. 36. 1.00 33.
9.0 136.0 0.0 0.0
9. 3.3 L.0 1.5
   131 7 2A A 3
                                                       €.3
                                                        1.0
         130.3
                                                                 .7+42731928596
         1.30
              333 146 4.44
0.0 106.6 6.4
133 64211
                                             37.
                                             1.7
                                   6.€
                                                         6.0
        100.0
                   7.
                                     9.0
                          0.1
                                                        1.0
                                                                 . 0555783291520
        1.20
```

ITEMIZED INPUT FOR AID *

* Extracted from McNichols [25]

Itemized Input for AID

1. Title Card

| Card Column(s) | Use | Description |
|-------------------|-----------|--|
| 1 | Card Type | Must contain the numeric value "1", |
| 2-49 | Job Title | Up to 48 alphabetic and/or numeric characters used to label the run. |
| 50 | IRUN | Numeric "0" for normal AID operation |
| 51–56 | NCPERM | Number of cases in the data file. May be omitted when data is from a disk or tape file. |
| 79–80 | IFMT | The number of cards used for the FORTRAN format statement (the next card or set of cards in the control card deck). Up to 4 cards may be used. |

FORTRAN Foramt Card(s)

| Card Column(s) | Use | Description |
|-------------------|----------------|--------------|
| 1-78 | Data Format | FORTRAN form |

ormat statement beginning with a left parenthesis and ending with a right parenthesis. Only integer fields of the form: Iw, where w is the number of characters used to describe a variable, can be specified. The characters: X can be used to skip columns, T to tab to a desired character position, and / to indicate the beginning of a new record for multiple record cases. Warning: be careful not to extend the format statement beyond column 78 as these characters are not processed by AID. If more than 78 characters are needed for the format statement, use another format card and change the count in column 80 of the title card.

APPENDIX C

Itemized Input for AID (cont'd)

3. <u>Description Card</u>

| Card Column(s) | Use | Description |
|-------------------|------------------------------|---|
| 1 | Card Type | Must contain the numeric value "3" |
| 2-6 | Stopping Rule:P1 | Minimum value of TSS_1/TSS_T to consider group i for splitting. (Section 8.2.2, paragraph 2). A decimal point is implied to the left of col. 2. |
| 7-11 | Stopping Rule:P2 | Minimum value of BSS_1/TSS_T to permit group i to split (Section 8.2.2, paragraph 3). A decimal point is implied to the left of column 7. |
| 12-16 | Stopping Rule MAXGP | Maximum number of subgroups into which the set of data will be split. |
| 17-21 | Stopping Rule: NMIN | Minimum number of observations which must be in a group after it is split. Value must be at least 2. |
| 22-26 | Iteration Print: KSTOP | Number of AID iterations for which detailed information will be printed. Only summary results for iterations will be output after this point. |
| 27-29 | No. of Variables NV | Specifies number of variables to be read from each case. This will be the total number of variables described by the format statement. |
| 33 | Rewind: KRW | Should be the numeric value "1" if input data is on a disk or tape file, left blank otherwise. |
| 34 | Missing Values: IOPT | Set to "1" if a case with <u>any</u> out-of-range predictor values is to be rejected, blank or zero otherwise. The "1" value is analogous to listwise deletion in SPSS, as far as the predictor variables are concerned. There is no capability in AID which corresponds directly to a pairwise deletion option. The IOPT setting must be considered when predictor cards (type 4) are coded. |

APPENDIX C

Itemized Input for AID (cont'd)

4.

23

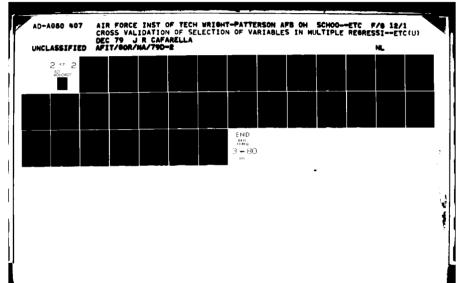
| Card Column(s) | <u>Use</u> | Description |
|-------------------|---------------------------|---|
| 37 | Input Medium: ICARD | If zero or blank, the data file is assumed to be a disk or tape file with the local file name "TAPE25". If set to "1", data is assumed to be on punched cards which follow the AID control cards. |
| 38 | Tree Control; ITREE | This parameter controls the output of computer printed tree diagrams summarizing the splits. If set to zero or blank, no diagrams are generated. If set to "1", only a detailed tree is generated. If set to "2", both a detailed and a skeleton tree will be produced. |
| Predictor Card | (s) | |
| Card Column(s) | Use | Description |
| 1 | Card Type | Must contain the numeric value "4" There will be one predictor card for each predictor variable to be used in the AID run. However, all predictors described by the format statement do not need to be used |

| | | run. However, all predictors described by the format statement do not need to be used in the AID run. The NV parameter (card 3) has a value associated with the number of variables described by the format statement, not the number of predictor cards used in the run. |
|------|-------------------|---|
| 2-19 | Predictor Name | Up to 18 alphabetic or numeric characters used to label the predictors in the AID output. |

| 20–22 | Field Number | A variable number which must correspond to the variable sequence provided by the format statement. This is, the third variable described by the format statement represents field number 3 for predictor variable numbering |
|-------|-----------------|---|
| | | purposes |

| | | blank | | | | | | |
|----|-------|--------|-------|-------|--------|--------|-------|------|
| as | nomi | nally | scale | ed, " | L" for | r var | iable | s to |
| Ъe | trea | ted as | ordi | nally | y scal | Led. | The | |
| ex | ample | in se | ction | 8.1 | 111u | strate | es th | e |
| | | of the | | | | | | |
| OT | dinal | varia | hles | in Al | rn. | | | |

Predictor Type: KBL1



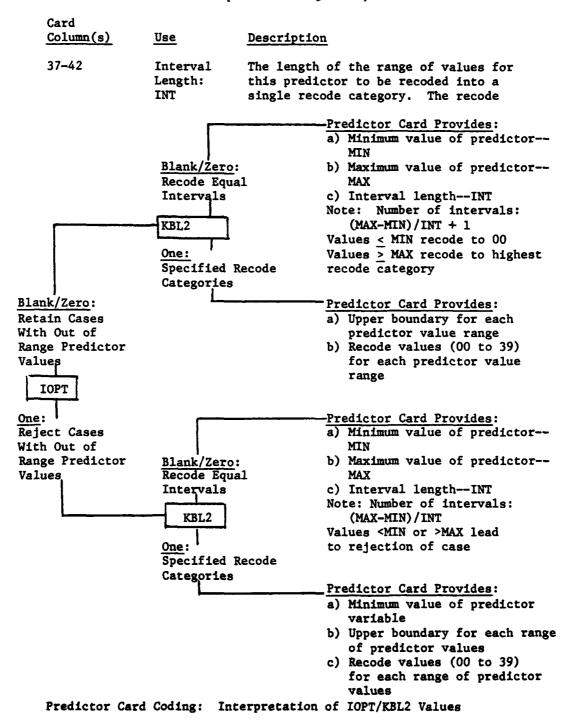
Itemized Input for AID (cont'd)

| Card Column(s) | <u>Use</u> | Description |
|-------------------|----------------------------|--|
| 24 | Predictor Definition: KBL2 | This parameter, used in conjunction with the IOPT value on card 3, tells AID how to interpret the values on the remainder of the predictor card. A zero value indicates that the range of possible values for this predictor variable will be divided into intervals of fixed length. A value of "1" means that the range of values for this predictor will be divided into intervals of varying length. When KBL2 is set to zero, minimum and maximum values and an interval length will be provided. When KBL2 is set to "1", boundaries for the intervals into which the range of predictor values will be divided will be specified. Figure 8.7 summarizes the interpretation of IOPT/KBL2 value combinations and should be referenced in choosing the desired values and predictor card format. |

A. IOPT Equal Zero and KBL2 Equal Zero:

| Card Column(s) | Use | Description |
|-------------------|-----------------------------------|---|
| 25-30 | Minimum Predictor Value:MIN | Predictor variable values <u>less than or equal</u> to this value will be recoded to an internal value (recode category) of 00. |
| 31-36 | Maximum Predictor Value:MAX | Predictor variable values greater than or equal to this value will be recoded to the highest recode category value used for this predictor. |

APPENDIX C



| Card Column(s) | Use | Description |
|----------------------|-----------------------------------|--|
| | | category assigned to a specific predictor value between the MIN and MAX value will be: |
| | | Recode Category= Predictor Value-MIN INT |
| | | The number of recode categories will be: |
| | | $NCAT = \frac{MAX - MIN}{INT} + 1$ |
| | | The highest numbered recode category will be NCAT-1, and values greater than or equal to MAX will be assigned this value. |
| 44-45 | | In a basic application of AID, each of |
| 53–54 62–63 | | these pairs of columns should contain the value "-1". These columns can be used in conjunction with other predictor card parameters to alter the recoding process by assigning specific recode categories to specific numeric values of the predictor variable. Since this is a less often used capability, it will not be discussed in detail here. |
| B. <u>IOPT Equal</u> | Zero and KBL | 2 Equal One: |
| 25–27 | Lowest Recode Category | A value between 00 and 39 which is the numeric value to be used internally by AID to represent predictor variable values less-than-or-equalto the first specified input value. |
| 28-33 | First Specified Input Value | A value of the predictor variableused with lowest recode category. |
| 34-36 | Second Recode Category | A value between 00 and 39 which is the value to be used internally by AID to represent predictor variable values strictly greater than the first specified input value, and less-than-or-equal-to the second specified input value. |

APPENDIX C

Itemized Input for AID (cont'd)

| Card | | |
|----------------------|---|--|
| Column(s) | Use | Description |
| 37-42 | Second Specified Input Value | A value of the predictor variable used in conjunction with the second recode category as the boundary of the predictor variable values to be recoded to the value specified by the second recode category. |
| 43-45 | Third Recode Category | A value between 00 and 39 which is the value to be used internally by AID to represent predictor variable values strictly greater than the second specified input value and less-than-or-equal-to the third specified input value. |
| 46-51 | Third Specified Input Value | A value of the predictor variableused in conjunction with the third recode category. |
| 52-54 61-63 | Fourth & Fifth Recode Categories | The descriptions of these field are comparable to those given for the first, second and third recode categories and specified input values. |
| C. <u>IOPT Equal</u> | one and KBL2 | Equal Zero: |
| 25-30 | Minimum Predictor Value:MIN | Predictor variable values strictly less than this value will cause the case to be rejected. |
| 31-36 | Maximum Predictor Value:MAX | Predictor variable values greater than or equal to this value will cause the case to be rejected. |
| 37-42 | Interval Length: INT | The length of the range of values for this variable to be recoded into a single recode category. The recode category assigned to a specific predictor variable between MIN and MAX will be: Predictor Value-MIN |
| | | Recode Category = Tredictor Value-MIN |

| Card | | · | | | | | |
|-------------------------|---------------------------------------|--|--|--|--|--|--|
| Column (s) | <u>Use</u> | Description | | | | | |
| | | The number of recode categories will be: | | | | | |
| | | $NCAT = \frac{MAX - MIN}{INT}$ | | | | | |
| 44-45 53-54 62-63 | | In a basic application of AID, each of these pairs of columns should contain the value"-1". These columns can be used in conjunction with other predictor card parameters to alter the recoding process by assigning specific recode categories to specific numeric values of the predictor variable. Since this is a less often used capability, it will not be discussed in detail here. | | | | | |
| D. <u>IOPT Equal</u> | One and KBL2 | Equal One: | | | | | |
| 25–27 | Recode Category | Used only when more than one predictor card is required to describe the predictor variable. On the first predictor card for a variable this field should be blank. | | | | | |
| 28-33 | First Specified Input Value | Predictor variable values less-than-or-equal- to this value will cause the case to be rejected. | | | | | |
| 34–36 | Second Recode Category | A value between 00 and 39 which is the value to be used internally by AID to represent predictor variable values strictly greater than the first specified input value, and less-than-or-equal-to the second specified input value. | | | | | |
| 37-42 | Second Specified Input Value | A value of the predictor variable associated with the second recode category. | | | | | |
| 43–45 | Third Recode Category | A value between 00 and 39 which is the value to be used internally by AID to represent predictor variable values strictly greater than the second specified input value and less-than-or-equal-to the third specified input value. | | | | | |

| | Card Column(s) | <u>Use</u> | Description |
|----|-------------------|--|--|
| | 46-51 | Third Specified Input Value | A value of the predictor variable associated with the third recode category. |
| | 52-54 61-63 | Fourth & Fifth Recode Categories | The descriptions of these fields are comparable to those given for the first, second, and third recode categories and specified input values. |
| 5. | Criterion Card | | |
| | 1 | Card Type | Must contain the numeric value "5" |
| | 2-19 | Criterion Name | Up to 18 Alphabetic or numeric characters used to label the criterion variable in the AID output. |
| | 20–22 | Field Number | A variable number which must correspond to the variable sequence provided by the format statement. That is, the third variable described by the format statement represents field number 3 for criterion variable identification purposes. The criterion variable does not have to be the field which is physically last in each case as long as the proper field numbers are used to identify predictors and the criterion. |
| | 23-24 | Weight Field | A variable number representing a weight field in each case, used to weight the values in AID computations. This field can be left blank, causing all cases to be equally weighted, and this is the normal mode of operation. |
| | 25-30 | Maximum Criterion Value: YMAX | If the criterion variable value is strictly greater than YMAX in a case, the case is rejected. Values up to "999999" can be specified for YMAX. |

APPENDIX C

Itemized Input for AID (cont'd)

| Card Column(s) | <u>Use</u> | Description |
|-------------------|--|--|
| 31-36 | Minimum Criterion Value: YMIN | If the criterion variable value is strictly less than YMIN in a case, the case is rejected. |
| 37-42 43-48 | Deletion Values: MD1,MD2 | If the criterion variable value is equal to either of these values, the case is rejected. If the use of deletion values is not desired, or only one deletion value is desired, setting MDl and/or MD2 to values outside the range of YMIN to YMAX deactivates their use. |

6. AID End-Of-Job Card

Card Type Must contain the numeric value "9".

Indicates the end of all of the AID control cards.

APPENDIX D

SELECTED AID OUTPUT

** UNIVERSATY OF TEXAS VERSION OF AIGH AS ATHRED FROM AFHAL, LACKLAND AFB ** MODIFIED FOR DROACER BY CAPT LL GOUGH, OCT 72

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APPENDIX E

SELECTED SPSS OUTPUT

PAGE 15.30.20. 12/03/79

VOGELBACK COMPUTING CENTER NORTHHESTERN UNIVERSITY

S P S S - - STATISTICAL PACKAGE FOR THE SOCIAL SCIENCES

VERSION 7.0 -- JUNE 27 1977

(2x, F 3, 0, 1 x, A6, 12(1x, F2, 0), 1x, F4, 0, F16, 13/ 3(4x, F16, 13)/3(4x, F16, 13)) REGRESSION LOGNENDATA CONTROL N, ID, X1 TO X20 DISK UNKNOWN PRINT BACK VACIABLE LIST INPUT HEDIUM N OF CASES INPUT FORMAT RUN NAME

69 "COLUMNS" ARE USED ON A RECORD. THE INPUT FORMAT PROVIDES FOR 22 VARIABLES. 22 WILL BE READ IT PROVIDES FOR 3 RECORDS (*CARDS*) PER CASE. A MAKIMUN OF

WARNING - A WUMERIC VARIABLE HAS A WIDTH GREATER THAN 14. SHALL ROUNDING/TRUNCATION ERRORS HAY OCCUR.

COMPUTE

COMPUTE X34=X13*X14 VARIABLES=X1 TO X34/ VARIABLESSION=X20 (22,1.0,0,0.0) WITH X2,X4,X5,X6,X10,X11,X14, X15,X17,X21 TO X34 (2)

STATISTICS AL READ INPUT DATA FINISH

00053600 CM NEEDED FOR REGRESSION

JPTION - 1 IGNORE MISSING VALUE INDICATORS

A COLOR OF THE WARRANT OF THE PARTY OF THE P

FILE NOMAME (CREATION DATE = 12/03/79)

| CASES | 7.1 | 7.7 | 7.7 | 7. | 71 | 71 | 7. | 7.1 | 71 | 71 | 71 | 7. | 7. | 71 | 7.1 | 71 | 7. | 7.7 | 7.7 | 7.1 | 71 | 12 | 7.7 | 7. | : | 71 | 71 | 71 | 71 | 71 | Z | 71 | 17 | 71 |
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| MEAN | 25 | .0423 | 8 | 23 | 3 | 045 | 920 | 53 | 760 | 2 | 5 | 8 | 20 | ž | .868 | 545 | 3 | .566 | .725 | 020 | 537 | .362 | Z | 20 | .150 | .811 | 743 | .542 | 8 | •69 | 999 | 2 | 3 | = |
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| .00500 | | | F 7.13752 | VARIABLES NOT IN THE EQUATION PARTIAL TOLERANCE | 00000 | | | | | |
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| .000000. F TO | | | OF SQUARES 176.57021 49.78910 | VARIABLE | X24 | | | | | |
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| 1.000000. | 1.79825 | SENT TO THE SENT T | VARIANCE RIABILITY | CON F | .22377333 | 1.9172841 | .62632328E-01 | 1,4074136 | 242° | .64 <i>8</i> 57393 .425 |
| 23 F TO ENTER | STD. DEV. | . | ANALYSIS CF REGRESSION RESIDUAL COEFF OF VAI | B STD ERROR 8 | 17.346404 | . 2555 2978 | 207-10304 | .83450842 | . 31751393 | .61187387 |
| MAXIMUM STEP 23 | . 8288 | RED ON STEP W | .88320 .78004 1.01847 | j | 9.2856518 1 | -, 35382193 | 59.533507 | . 99661459 | .12660075 | . +9276764. |
| PARAHETERS HA | HEAN RESPONS? | VARIABLE (S) ENTERED ON STEP NUMBER | MULTIPLE R R Schare Agjusted r Sjuare Sto deviation | VARIABLE | x2 9.2 | 58 BEX | | • | X11 .12 | 64° 22× |
| • | * | 106 | I K < W | · > | × | × | × | × | × | × |

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DEPENDENT VAZIABLE..

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| | • | | | | -4.21 |
| ٠: | x32 | 531.35247 | 667.96390 | .63278973 | .40 63 |
| | | | | -430 | 12.057 |
| | XIL | 1102.0708 | 280,38031 | 15.458658 | • 36 22 |
| • | | | | 000. | 246.667 |
| , , | X22 | 13099197 | . 22804494 | .32995024 | 2410 |
| | | | | .558 | -15.47 |
| | X15 | . 36000615 | . 17946696 | 4.0239337 | . 34 32 |
| ٠. | | | | .091 | 177.63 |
| | X17 | . 60315963 | . 43885436 | 1.8889640 | .3725 |
| | | | | •176 | 86.517 |
| | ×8 | -1.3736140 | 2,5219780 | .29665167 | 3815 |
| | | | | 658 0 | -38.69 |
| | X33 | .55957127E-01 | . 26894300 | .37504765E-01 | .0531 |
| | | | | 249. | 3.76 |
| ٠. | X 29 | 13546127 | 43869986 | .96757322E-01 | 1173 |
| | | | | 757 | -14.53 |
| | X21 | . 130 88 302 | . 15751183 | .68204793 | . 3564 |
| | | | | 6413 | 23.00 |
| | X10 | 2.6000225 | 1.6961873 | 2.3496684 | .7157 |
| | | | | .132 | 53.097 |
| | X31 | 36370529 | . 46191312 | .61993136 | 4143 |
| | | | | 435 | -12,09 |
| | X25 | 75005236 | 2 • 6 27 19 34 | .81507780E-01 | -,3021 |
| | | | | .776 | -5.651 |
| | X26 | 14280299 | .60250900 | .56175572E-01 | 27357 |
| | | | | .614 | -27.21 |
| | X23 | 34773056 | 1.1390687 | .93193562E-01 | 43737 |
| | | | | .761 | -6.13 |
| | (CONST ANT) | -10.438349 | 1.4928598 | 48.890528 | |
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and the second formation of the first of the second second

NOTE- 1 VARIABLES WERE NOT FORCED DUE TO INSUFFICIENT TO ERANGE. INCLUSION LEVELS WERE SET TO ZERO.

ALL VARIABLES ARE IN THE EQUATION.

REGRESSION * * * * *

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FILE NONAHE (CREATION DATE = 12/03/79)

REGRESSION . DGNEWDATA

X 20

DEPENDENT VARIABLE..

COEFFICIENTS AND CONFIDENCE INTERVALS.

| VARIABLE | | STD ERROR B | - | 95.0 PCT CONFIDENCE INTERVAL | FIDE | NCE INTERVAL |
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| X2 | 8.2056518 | 17.346404 | . 47304686 | -26.671625 | • | 43.082944 |
| BE X | 35362193 | . 2555 2978 | -1.3846603 | 86759899 | • | .15995513 |
| ₩X | 59.533507 | 207.10304 | . 28745839 | -356.87507 | • | 475.94208 |
| XS | . 99001459 | . 83450842 | 1.1203446 | 687R7706 | - | 2,6679062 |
| X11 | .12680075 | . 31751393 | . 399.35493 | 51160379 | • | .76520529 |
| X27 | . 49276704 | .61197387 | . 805 340 68 | 73746784 | • | 1.7230219 |
| X 28 | .64676379E-01 | . 13617898 | . 46 0 6 236 | 21315108 | • | .34250384 |
| *× | 3 32 67 319 | . 39887747 | 83:52470 | -1.1348700 | • | .46912381 |
| X32 | 531,35247 | 667,96390 | . 705 48 B81 | -811.67898 | • | 1874.3839 |
| X14 | 1102-0706 | 280.30031 | 3.9317500 | 538.4892ñ | | 1665.6523 |
| X22 | 13095197 . | . 22804494 | -, 571.41295 | 56956705 | • | .32752312 |
| x15 | . 36000615 | . 17946696 | 2 .0 0 5 9 7 4 5 | 83636371E-03 | 03. | .72084567 |
| X17 | . 56312963 | . 4 368 5436 | 1.3743959 | 27321622 | | 1.4855355 |
| 8 × | -1.3736140 | 2.5219780 | 54/165739 | -6.4443906 | | 3.6971627 |
| X 33 | .55957127E-01 | . 28894330 | . 19366147 | 52500172 | • | .63691598 |
| X 29 | 13646127 | 43869986 | - 31105839 | -1.0185265 | • | .74560392 |
| X21 | .13008302 | . 1575 1183 | . 82586193 | 10561574 | • | .44678178 |
| X10 | 2.6300225 | 1.6961873 | 1.5328628 | 81039070 | • | 6.0164356 |
| X31 | 36370529 | . 46191312 | 78738895 | -1.2324439 | • | .56503330 |
| X 25 | 75005236 | 2 . 6271934 | 28549567 | -6.0323788 | • | 4.5322741 |
| X26 | 14280299 | . 60250900 | 23701397 | -1.3542285 | • | 1.0660226 |
| X23 | 34773058 | 1.1390687 | 30527621 | -2,6379817 | • | 1.9425206 |
| CONSTANT | -10.438349 | 1.4928598 | -5 .9921834 | -13.439945 | • | -7.4367536 |

| REGRES SI ON | _ | .OGNEWDATA | | 12/03/79 | 15.30.20. | PAGE | O II |
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DEPENDENT VARIABLE. X20

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APPENDIX F

SELECTED LEAPS AND BOUNDS OUTPUT

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VITA

Joseph Richard Cafarella, Jr. was born on November 27, 1956 in Moses Lake, Washington. He graduated from Northern Burlington Regional High School in New Jersey in 1974 and attended the Virginia Military Institute where he graduated in 1978 with a Bachelor or Science degree and a double major in Mathematics and Civil Engineering and a reserve commission in the United State Air Force. In June of 1978 he entered the Air Force Institute of Technology.

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19. KEY WORDS (Continue on reverse side if necessary and identify by black number)

Cross Validation Selection of Variables Multiple Regression

20. ASSTRACT (Continue on reverse side it necessary and identity by block number)

Techniques and criterion for selection of the "best" subset of variables to be used in a regression model are reviewed.

A model was developed using the Automatic Interaction Detection (AID) algorithm as a pre-screening device for locating those variables most important to the regression including interaction terms.

Five previous models including the one developed by AID and one developed by Westinghouse on avionic characteristic data are used in cross validation experiments to determine the predictive power of these models on a new set of

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data points using the same set of variables. A cross validation ${\ensuremath{\mathbb{R}}}^2$ value is discussed as a criterion for choosing between competing models.